



# International Agreement Report

## Assessment of RELAP5/MOD3.3Beta Code for the LOFT Experiment L9-1/L3-3

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# **Assessment of RELAP5/MOD3.3Beta Code for the LOFT Experiment L9-1/L3-3**

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## **ABSTRACT**

The purpose of this report is to assess the capability of the RELAP5/MOD3.3Beta computer code to simulate thermal-hydraulic behavior associated with the LOFT Experiment L9-1/L3-3. The Experiment L9-1/L3-3 was a simulation of the total loss-of-feedwater accident and its recovery modes. Experiment L9-1 simulated a loss-of-feedwater accident with delayed reactor scram and no auxiliary feedwater injection. The loss-of-feedwater accident led to a loss-of-coolant accident through the PORV cycling operation.

Generally, the RELAP5/MOD3.3Beta calculation results were in good agreement with the L9-1 experimental data. The discrepancies between the calculation and the experiment were also identified in the temperature behaviors of the SG secondary side after dryout of the SG. However, these discrepancies were not considered to be significant, since the SG was in a de-coupled state from the PCS after the dryout of the SG secondary side.

Experiment L3-3 simulated two recovery modes from the loss-of-feedwater accident L9-1 without the aid of the emergency core coolant system. The first recovery mode consisted of turning off the primary coolant pumps and latching open the PORV to depressurize the primary system. The second mode consisted of refilling the SG to restore the secondary heat sink and removing decay heat through the feed-and-bleed operation using the secondary side of the SG.

The general trends observed in Experiment L3-3 were similar to those of the RELAP5/MOD3.3Beta code calculations. In addition, some differences between the code calculations and the L3-3 experimental data were observed. The code predicted excessive swelling of the PCS fluid during the first recovery mode, and predicted excessive cooling during the second recovery mode. The differences during the first recovery mode were due to the code's under-estimation of total discharged energy through the PORV. For the discrepancies during the second recovery mode, the code modeling deficiency of the SG secondary side was presumed to be one of the reasons. However, it is concluded that further investigation into the deviation sources are needed to enhance the code's predictability, since the specific reasons for the deviation were not clearly identified in this assessment.

Sensitivity studies show that several parameters have significant effect on the predicted thermal-hydraulic behaviors. These parameters include the pressurizer spray system loss coefficient, nodalization of the SG secondary side, SG U-tube heat transfer area, heat transfer coefficient from the LOFT main components to the environment, and the PORV discharge coefficient. The first three parameters are significant during the short-term transient phase, while the last two are significant during the long-term transient phase. Therefore, the five parameters listed above should be carefully modeled to obtain appropriate calculation results for transient types such as the total-loss-of feedwater accident and its recovery modes.



## **FOREWORD**

This report is prepared to assess the capability of the RELAP5/MOD3.3Beta computer code to simulate thermal-hydraulic behavior associated with the LOFT Experiment L9-1/L3-3. The RELAP5 computer code has been developed as a highly generic best-estimate code to be used for simulation of a wide variety of hydraulic and thermal transients in LWR systems. As one of the new code version, RELAP5/MOD3.3Beta was released in June 2001 with several new models and improvements to existing models.

The Loss-of-Fluid Test (LOFT) integral experimental facility was a scaled model of a commercial pressurized water reactor (PWR) to model the nuclear, and thermal-hydraulic phenomena expected to occur primarily during a loss-of-coolant accident (LOCA). The Experiment L9-1/L3-3 was performed in 1981 as a part of the LOFT Experimental Program to simulate total loss-of-feedwater accident and its recovery modes.

The code-predicted results were compared with experimental data to assess the code predictability. From the comparisons, it is concluded that the RELAP5/MOD3.3Beta computer code has sufficient capability in predicting the thermal hydraulic phenomena occurred in the LOFT Experiment L9-1/L3-3 because the code-predicted results were generally in agreement with the measured data. However, some discrepancies between the calculation and the experiment were also observed. In addition, major parameters having significant effect on the predicted thermal-hydraulic behaviors were identified through sensitivity studies.

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## **EXECUTIVE SUMMARY**

The RELAP5 computer code has been developed as a highly generic best-estimate code to be used for simulation of a wide variety of hydraulic and thermal transients in LWR systems. As one of the new code version of the RELAP5, RELAP5/MOD3.3Beta was released with several new models and improvements to existing models. The purpose of this report is to assess the capability of the RELAP5/MOD3.3Beta computer code to simulate thermal-hydraulic behavior associated with the LOFT Experiment L9-1/L3-3.

The Experiment L9-1/L3-3 was a simulation of the total loss-of-feedwater accident and its recovery modes. In Experiment L9-1, the pressure increase in the primary system due to the power-cooling mismatch was controlled by the cycling operation of the pressurizer spray valve and by the coolant discharge through the power-operated relief valve (PORV). In the subsequent Experiment L3-3, two independent recovery procedures for the removal of the core decay heat during the total loss-of-feedwater accident were investigated. The first recovery procedure was the PORV latching open to depressurize the primary coolant system. The second one was accomplished by refilling the steam generator to restore the secondary side heat sink and removing the decay heat through a feed-and-bleed operation using the steam generator secondary side.

For the assessment calculation, the base input decks were prepared by incorporating the major parameters which were identified through sensitivity studies to have significant effect on the code calculation results. The code-predicted results were compared with the experimental data to assess the code predictability. Major conclusions through this assessment are summarized as follows:

- From the comparisons presented with Figures and Tables, it was shown that the code-predicted results were generally in agreement with the measured data. Therefore, it is concluded that the RELAP5/MOD3.3Beta computer code has sufficient capability in predicting the thermal hydraulic phenomena occurred in the LOFT Experiment L9-1/L3-3.
- However, the discrepancies between the calculation and the experiment were also identified. In Experiment L9-1, the code over-estimated temperature behaviors of the SG secondary side after dryout of the SG. However, these discrepancies were not considered to be significant, since the SG was in a de-coupled state from the PCS after the dryout of the SG secondary side. In Experiment L3-3, the code predicted excessive swelling of the PCS fluid during the first recovery mode, and predicted excessive cooling during the second recovery mode. The differences during the first recovery mode were due to the code's under-estimation of total discharged energy through the

PORV. For the discrepancies during the second recovery mode, the code modeling deficiency of the SG secondary side was presumed to be one of the reasons. However, it is concluded that further investigation into the deviation sources are needed to enhance the code's predictability, since the specific reasons for the deviation were not clearly identified in this assessment.

- Through sensitivity studies, the major parameters were identified to have significant effect on the predicted thermal-hydraulic behaviors. These parameters include the pressurizer spray system loss coefficient, nodalization of the SG secondary side, SG U-tube heat transfer area, heat transfer coefficient from the LOFT main components to the environment, and the PORV discharge coefficient. The first three parameters are significant during the short-term transient phase, while the last two are significant during the long-term transient phase. Therefore, the five parameters listed above should be carefully modeled to obtain appropriate calculation results for transient types such as the total-loss-of feedwater accident and its recovery modes.

## 1. INTRODUCTION

The RELAP5 computer code has been developed as a highly generic best-estimate code to be used for simulation of a wide variety of hydraulic and thermal transients in LWR systems. As one of the new code version of the RELAP5, RELAP5/MOD3.3Beta was released in June 2001 with several new models and improvements to existing models [1]. The purpose of this report is to assess the capability of the RELAP5/MOD3.3Beta computer code to simulate thermal-hydraulic behavior associated with the LOFT Experiment L9-1/L3-3.

The Loss-of-Fluid Test (LOFT) integral experimental facility was a scaled model of a commercial pressurized water reactor (PWR). The purpose of this facility was to model the nuclear, and thermal-hydraulic phenomena expected to occur primarily during a loss-of-coolant accident (LOCA). In general, coolant volumes and flow areas in the LOFT were scaled using the ratio of the core power of 50 MWth in the LOFT to 3,000 MWth in a commercial PWR.

The Experiment L9-1/L3-3 was performed in 1981 as a part of the LOFT Experimental Program. It was a simulation of the total loss-of-feedwater accident and its recovery modes. The total loss-of-feedwater (TLOFW) accident is a beyond-design-basis-accident initiated by a loss-of-feedwater due to the failure of the main feedwater pump and subsequent no auxiliary feedwater injection. During the total loss-of-feedwater accident, heat removal capability in the secondary side of the steam generator (SG) is completely degraded and pressure and temperature of the primary coolant system (PCS) are increased to the reactor scram set point. Following the reactor scram, the core decay heat should be removed by proper controlling methods to prevent severe core damage. The role of core decay heat removal during the total loss-of-feedwater accident was considered important since it was identified as one of the major contributors to the severe core damage frequency in previous studies such as WASH-1400 [2].

The LOFT Experiment L9-1/L3-3 provided experimental data for several methods of removing the decay heat during the total loss-of-feedwater accident and its recovery phases. In Experiment L9-1, the pressure increase in the primary system due to the power-cooling mismatch was controlled by the cycling operation of the pressurizer spray valve and by the coolant discharge through the power-operated relief valve (PORV). In the subsequent Experiment L3-3, two independent recovery procedures for the removal of the core decay heat during the total loss-of-feedwater accident were investigated. The first recovery procedure was the PORV latching open to depressurize the primary coolant system. The second one was accomplished by refilling the steam generator to restore the secondary side heat sink and removing the decay heat through a feed-and-bleed operation using the steam generator secondary side. During the second procedure, the primary system pressure decreased rapidly after the reestablishment of the steam generator heat removal capability, and the heat generated in the reactor core was transferred to the steam generator by two-phase natural circulation [3]. In short, the LOFT L9-1/L3-3 was an experiment to evaluate the effectiveness of the PORV and the feed-and-bleed operation using the secondary side for removal of decay heat. This experiment has also been used as a means to evaluate the ability of a thermal-hydraulic computer code in predicting major phenomena.

For the assessment calculation, the base input decks were prepared based on available RELAP5 assessment [4] for this experiment. The major parameters, which were identified through sensitivity studies to have the most significant effect on the predicted thermal hydraulic behaviors, were incorporated into the base calculation to improve the code predictability. The

code calculation results were then compared with the measured data to assess the code capability of predicting major phenomena.

## 2. FACILITY AND TEST DESCRIPTION

### 2.1 Facility Description

The LOFT integral experimental facility was a scale model of a commercial PWR. The purpose of this facility is to model the nuclear, and thermal-hydraulic phenomena expected to occur primarily during a LOCA. In general, coolant volumes and flow areas in the LOFT were scaled with a ratio of the 50 MWth LOFT core to a commercial 3,000 MWth PWR core. Also, components used in the LOFT are similar to those of a commercial PWR [3]. The experimental facility included five major subsystems which had been instrumented such that system variables could be measured and recorded throughout the experiment. The subsystems include (a) the reactor vessel, (b) the intact loop, (c) the broken loop, (d) the blowdown suppression system, and (e) the emergency core cooling system (ECCS) [5]. The major components of the LOFT facility are shown in Figure 1, and a detailed system description is presented in Reference [6].

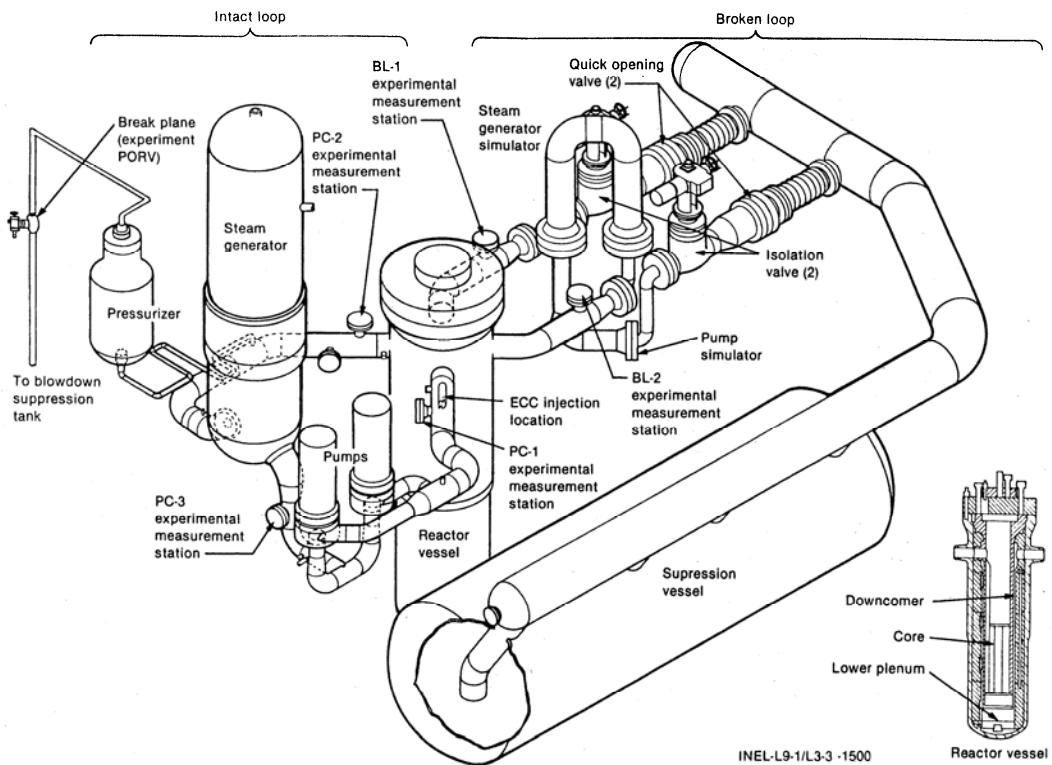


Figure 1. Configuration of LOFT System for Experiment L9-1/L3-3

### 2.2 Test Description

Since 1976, 43 non-nuclear and nuclear experiments have been performed in the LOFT facility

[3]. The Experiment L9-1/L3-3 [3,5,7] conducted on April 15, 1981, consisted of two sequential tests. Experiment L9-1 was performed as part of the LOFT Experiment Series L9 (anticipated transient with multiple failure), and Experiment L3-3 was performed as part of the LOFT Experiment Series L3 (small break LOCA).

Experiment L9-1 was the first anticipated transient with multiple failures performed in the LOFT, and simulated a loss-of-feedwater accident with delayed reactor scram and no auxiliary feedwater injection. The loss-of-feedwater accident led to a loss-of-coolant accident through the PORV. In Experiment L9-1, the transient was initiated by loss-of-feedwater due to the failure of the main feedwater pump. The reactor scrammed on the indication of high pressure (15.745 MPa) in the intact loop hot leg approximately 65 seconds after the main feedwater pump was tripped. The auxiliary feedwater injection into the steam generator was prevented, as was scram on the indication of low liquid level in the steam generator. The main steam control valve (MSCV) of the steam generator started to close automatically on the reactor scram and finished closing 12.2 seconds later (at 77.2 sec). The pressurizer spray valve cycled automatically at its close (15.05 MPa) and open (15.338 MPa) set points from 30 seconds until it was closed by the operators at the 1,246.0 seconds to allow the PCS pressure to increase to the PORV set point. The PORV started cycling operation at 1,467.9 seconds to control primary system pressure, until it was manually latched open at 3,270 seconds. The open and close set points of the PORV were 16.20 MPa and 16.06 MPa, respectively.

Experiment L3-3 simulated two recovery modes from the loss-of-feedwater accident L9-1 without the aid of emergency core coolant (ECC). The first recovery mode consisted of turning off the primary coolant pumps and latching open the PORV to depressurize the primary system. The second mode consisted of refilling the steam generator to restore the secondary heat sink and removing decay heat through the feed-and-bleed operation using the secondary side of the steam generator. Experiment L3-3 began when the PORV was secured in the open position. The primary coolant pumps were tripped 15 seconds later, with pump coastdown lasting about 20 seconds. Saturation occurred in the upper plenum about 60 seconds after the beginning of Experiment L3-3 at the 3,329.4 seconds. The primary pressure decreased to the saturation pressure of 12.3 MPa. This pressure was below the high pressure safety injection system (HPSI) set point of 13.2 MPa, which would have initiated ECCS injection had it not been purposely locked out. After closing the PORV at 4,849.7 seconds, steam generator refill began at 5,114.6 seconds. Natural circulation was established during steam generator refill which was completed at 5,746.4 seconds. Alternating secondary coolant system feed-and-bleed operations began at the 6,712.2 seconds. The experiment was complete at 9,517.4 seconds. The initial plant operating conditions and the major sequence of events for Experiment L9-1/L3-3 are presented in Table 1 and 2, respectively.

The objectives of the L9-1/L3-3 Experiment were specified as follows [5]:

#### 2.2.1.1 *Experiment L9-1 Objectives*

- To evaluate uncertainties in predicted primary and secondary thermal hydraulic response associated with steam generator dryout during delayed scram,
- To evaluate the adequacy of PORV to provide overpressure protection in a loss-of-feedwater accident.

#### *2.2.1.2 Experiment L3-3 objectives*

- To investigate uncertainties in system response during a PORV imposed small break with loss of secondary heat sink,
- To assess uncertainties in small break performance predictions identified in NUREG-0623 [8],
- To assess the effectiveness of steam generator refill on loss-of-feedwater accidents following reestablishment of auxiliary feedwater availability,
- To assess the relative magnitude of the change in reactor vessel mixture level as a result of primary coolant system shrink during steam generator refill,
- To contribute to the NRC relief and safety valve testing program by providing experimental data on PORV performance characteristics over a range of PORV inlet fluid conditions.



### **3. CODE AND MODELING**

#### **3.1 Code Description**

The code version of RELAP5/MOD3.3Beta, into which several new models and improvements were incorporated, was used for this assessment calculation. Some models recommended in the previous RELAP5 versions such as a new steam table and the Henry-Fauske choked flow model were used as default models in this version. In addition, improved or modified models in the RELAP5/MOD3.3Beta include non-condensable gas treatment, wall friction term modification, time-dependent volume correction, CANDU model updates, etc. The descriptions of the RELAP5/MOD3.3Beta code are presented in detail in the code manuals [1].

#### **3.2 Base Input Modeling**

For the purpose of the RELAP5/MOD3.3Beta assessment, input decks for the base calculation were prepared based on the reference calculation [4] which was the recent RELAP5 assessment for the LOFT Experiment L9-1/L3-3. The modifications were made to the reference input decks to incorporate the major parameters which were identified through sensitivity studies to have significant effect on the code calculation results. These parameters include loss coefficient of the pressurizer spray system, nodalization of the secondary side of the steam generator, heat transfer area of the steam generator U-tube, heat transfer coefficient from the LOFT main components to the environment, and discharge coefficient of the PORV. The results of the sensitivity studies for the parameters listed above are presented in Section 4.2.

The modifications made to the reference input decks for base input modeling are summarized as follows:

- The mass flow rate into the pressurizer through the pressurizer spray valve was increased by reducing the loss coefficient of the pressurizer spray system
- The bottom node of the steam generator secondary side and associated nodes of the U-tube of the reference calculation were subdivided into four, which implies that the number of nodes of the SG secondary side associated with the U-tube changed into six.
- The heat transfer area of all the nodes of the steam generator U-tube increased by 20% to improve the code-predicted heat transfer phenomena through the SG U-tube.
- The heat transfer coefficient to the environment from the LOFT main components (the reactor vessel, the steam generator, the pressurizer, and primary coolant system) was increased by 40% to have the PCS temperature match with the experimental data during the long-term phase of the transient.

- The discharge coefficient and the thermal non-equilibrium constant of the PORV were set to 0.8 and 0.03 respectively to make the code-calculated mass flow rate through the PORV be in agreement with test data.
- The counter current flow limitation (CCFL) model was applied to the junctions (components 115-3, 400-1, 410-0) for which the flooding phenomena was presumed to occur.
- The additional junction connected to the accumulator was removed, because it was not allowed in the code version of RELAP5/MOD3.3Beta. Since the emergency core cooling system (ECCS) was not injected during Experiment L9-1/L3-3, the junction removal from the accumulator does not affect the calculation results.
- The initial conditions in the reference input decks for some volumes were slightly modified to make the base input decks compatible with the RELAP5/MOD3.3Beta code.

As shown in Figure 2, the LOFT facility was composed of 134 volumes, 143 junctions, and 142 heat structures in the RELAP5 modeling for the base calculation. The intact loop was modeled with 31 hydrodynamic volumes. Environmental heat losses from all the piping metal structures exposed to atmosphere were simulated using the heat structure components. The broken loop was composed of a hot leg, a cold leg, a SG-pump simulator, a reflood assist bypass system (RABS), and quick opening blowdown valves (QOBVs). The volume and junction modeling options were set to the default options. The active core, the downcomer and the filler gap were composed of three volumes, six, and seven vertically stacked volumes, respectively. The rod bundle interphase friction model option was applied to the active core volumes. The fuel rods were modeled using 3 heat structures representing the central fuel assembly and 2 heat structures representing the peripheral fuel assemblies of the LOFT core. The pressurizer system was modeled with a surge line, a pressurizer vessel, a spray line from the cold leg, a spray valve and a PORV. Two volumes for the surge line, nine volumes for the pressurizer vessel and one volume for the spray line were used. The spray valve and the PORV were simulated with two trip valves. The associated trip logic was prepared according to the experimental specification. The SG was modeled using 12 volumes in the primary coolant system and 8 volumes in the SG riser. Heat was exchanged between the primary and secondary sides of the SG through the U-tube, which was modeled using 12 heat structures. The rod bundle interfacial friction option was used for the volumes in contact with the U-tubes heat structures. The emergency core cooling system in the LOFT was also modeled. However, it is not used in the transient calculation. The containment was modeled using a time-dependent volume with constant pressure.

A steady state run was performed to obtain initial conditions of the whole system prior to running the transient case. The initial conditions obtained from the steady state run are presented in Table 1 and compared to the measured data. The RELAP5 results for the steady state run agree well with the experimental initial conditions except for the hot leg temperature of the broken loop. The hot leg temperature of the broken loop deviated from the range of the experimental uncertainty. However, considering that the broken loop does not play an important role from the perspective of the heat removal and the temperature deviation was not significant, it was concluded that the out-of-range value for the broken hot leg temperature would not adversely affect the overall transient calculation.

The boundary conditions and the control trips used in the base calculation were identical to those used in the reference calculation. The information for the boundary conditions and the control trips can be found in the attached input decks. The steady state and the transient input decks for the base calculation are presented in Appendix A and B, respectively.

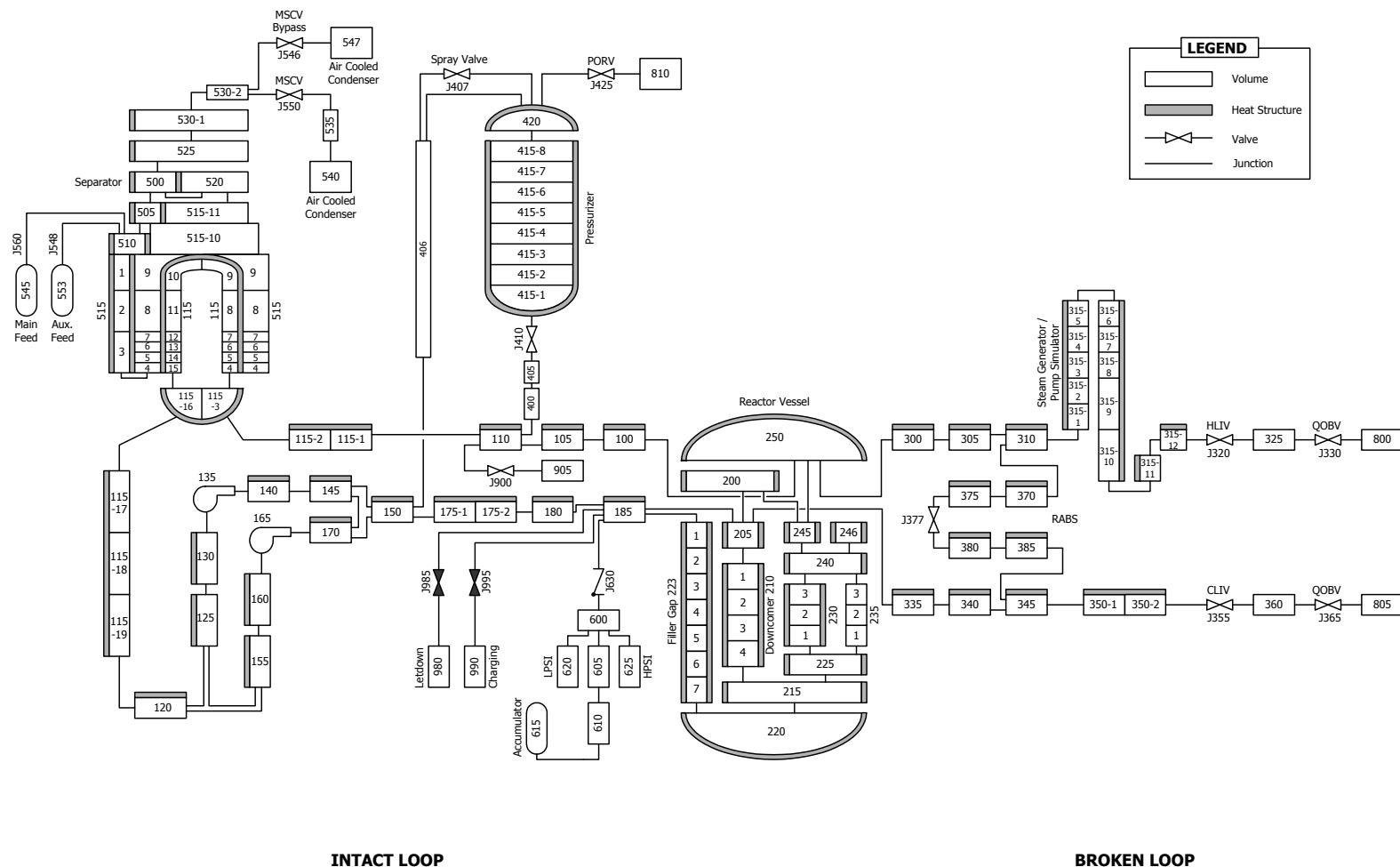


Figure 2. RELAP5 Nodalization for LOFT L9-1/L3-3

Table 1. Initial Condition for Experiment L9-1/L3-3

Parameter	Measured	Calculated
<b>Primary Coolant System</b>		
Mass flow rate (kg/s)	479.1±2.6	479.4
Hot leg pressure (MPa)	14.9±0.10	14.91
Cold leg temperature (K)	558.9±1.3	557.7
Hot leg temperature (K)	578.2±1.8	577.0
<b>Reactor</b>		
Power level (MW)	49.6±0.9	49.6
<b>Steam Generator Secondary Side</b>		
Water level (m)	0.14±0.08	0.14
Water temperature (K)	545.0±0.8	546.1
Pressure (MPa)	5.67±0.08	5.70
Mass flow rate (kg/s)	27.0±1.0	26.1
<b>Broken Loop</b>		
Hot leg temperature (K)	563.3±2.6	556.9
Cold leg temperature (K)	557.6±2.6	557.6
<b>Pressurizer</b>		
Steam Volume (m <sup>3</sup> )	0.43±0.05	0.48
Liquid volume (m <sup>3</sup> )	0.50±0.05	0.48
Water temperature (K)	614.9±1.3	614.7
Pressure (MPa)	14.93±0.25	14.93
Liquid level (m)	0.92±0.1	0.92



## 4. RESULTS AND DISCUSSION

### 4.1 Base Calculation

The results of the base calculation with the RELAP5 modeling described in the previous section are compared with the experimental data in Figures 3 through 13. Figures 3 to 7 are comparisons for short-term responses up to 300 seconds, while Figures 8 to 13 are comparisons for the long-term transient up to 10,000 seconds. In addition, the chronology of the major events for the base calculation is compared with the measured data in Table 2 for the LOFT Experiment L9-1/L3-3.

#### 4.1.1 Short-term Responses

The major thermal-hydraulic phenomena which can be observed during the short-term phase of the transient include, dryout of the SG secondary side, PCS pressurization, PCS pressure control by the pressurizer spray valve, and decay heat removal following reactor trip, etc.

The pressure trend of the PCS together with that of the SG secondary side is compared with experimental data in Figure 3. As the heat removal capability in the SG secondary side degraded due to the trip of the main feedwater pump, the pressure of the PCS gradually increased. When the PCS pressure reached the set pressure of 15.338 MPa, it was controlled by the pressurizer spray valve activation. As the heat generation in the reactor core exceeded the heat removal capability by both the SG secondary side and the pressurizer spray valve actuation, the PCS pressure continued to increase up to the reactor scram set pressure of 15.745 MPa. Following the scram, the PCS pressure decreased because the power input to the PCS dropped sharply to the decay power level. After that, the pressurization of the PCS due to decay heat was controlled by pressurizer spray actuation and subsequent steam condensation. The pressure of the SG secondary side rose gradually following initiation of the transient due to heating from the primary side. As the secondary side of the SG was drying out, however, the reduced heat removal capability decreased the pressure in the SG. The SG pressure increased again as the main steam control valve (MSCV) started to close on the reactor scram signal. As shown in Figure 3, the code pressure results calculated for both the PCS and the SG secondary side were in agreement with the experimental data.

The temperature comparisons of the calculated and experimental results for the PCS and the SG secondary side are shown in Figure 4. It is shown in the figure that the temperature behavior is predicted well by the code, even though minor discrepancies are shown. However, these differences are not considered significant to affect the later calculation results.

Figure 5 shows a comparison of the calculated reactor power to the experimental data. It is apparent that the predicted behavior of the reactor power is very similar to the experimental data. This implies that the code-predicted heat addition to the PCS during the transient matched well with the experiment.

A comparison of the experimental and calculated mass flow rate through the MSCV is presented in Figure 6. As the pressure in the SG secondary side increased, the mass flow rate through the MSCV increased until the MSCV started to close on the reactor scram signal. From this comparison, it can be stated that the mass flow rate behavior through the MSCV can be

predicted very well by the code.

Figure 7 shows a comparison of the calculated and experimental results for the SG collapsed liquid level. The SG secondary collapsed water level is a good indication of SG secondary conditions changing. The water level of the SG secondary side dropped monotonically due to evaporation without feed. As the water level decreased, the heat transfer rate through the SG U-tube degraded and this forced the PCS pressure to increase up to the reactor scram set point. After dryout of the SG secondary side, the heat transfer to the SG secondary side through the U-tube was by vapor natural circulation with a small wall heat transfer coefficient. This implies that the secondary system was de-coupled from the primary side and therefore it could no longer control the PCS pressurization. The calculated dryout rate of the SG secondary side closely resembled the test data as shown in Figure 7.

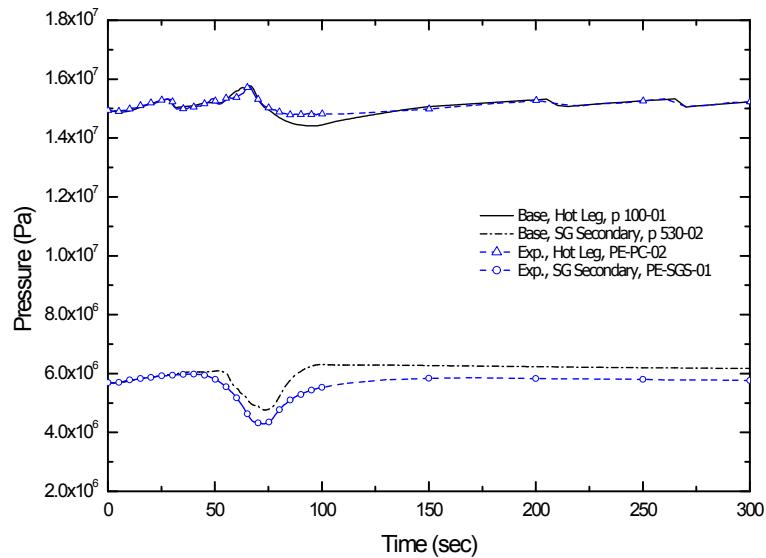


Figure 3. Comparison of Pressure for Short-term Response

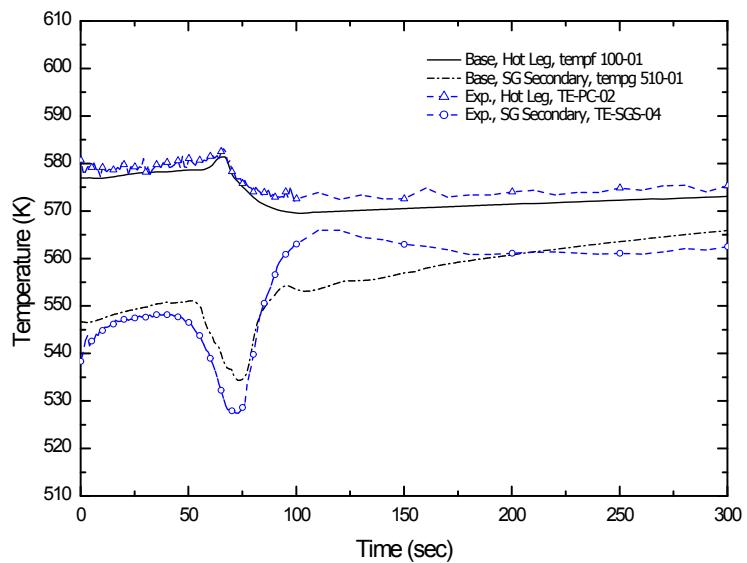


Figure 4. Comparison of Temperature for Short-term Response

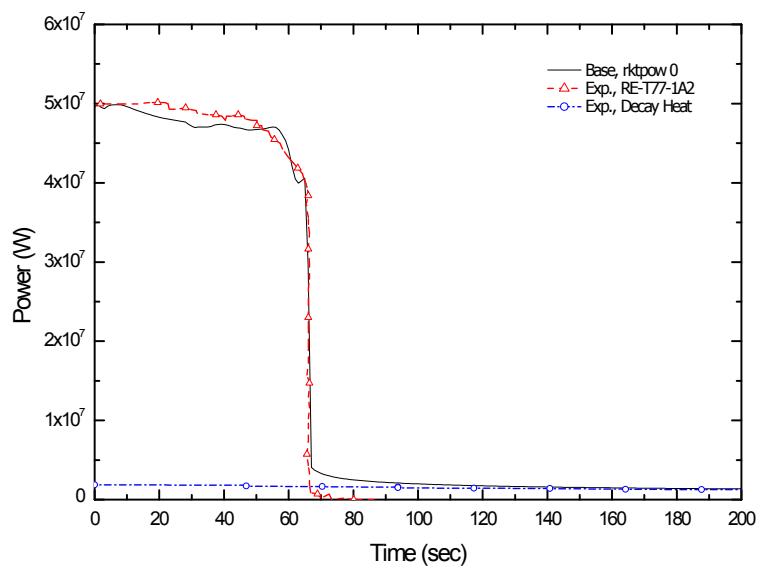


Figure 5. Comparison of Reactor Power for Short-term Response

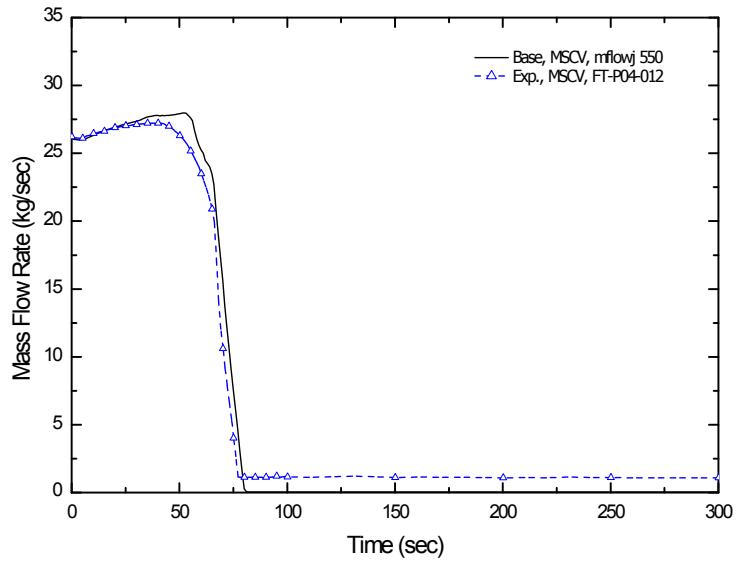


Figure 6. Comparison of Mass Flow Rate through MCV for Short-term Response

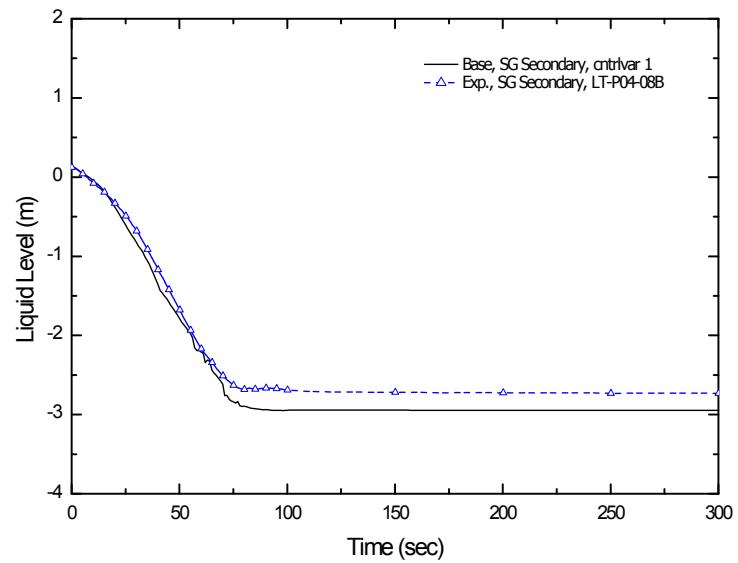


Figure 7. Comparison of SG Liquid Level for Short-term Response

Table 2. Major Sequence of Events for Experiment L9-1/L3-3

Event	Measured (sec)	Calculated (sec)
<b>L9-1</b>		
Main feedwater pump tripped off	0.0	0.0
Pressurizer spray activated	30.0±0.1	29.0
Reactor scram	65.4±0.2	65.0
Steam generator main steam control valve closed	77.2±0.2	80.0
Steam generator liquid level reached bottom of indicating range (0.25 m, above tube sheet)	190	71.0
Pressurizer spray valve cycling initiated	208.9±0.1	205.0
Pressurizer liquid level reached top of indicating range (1.83 m, above bottom)	1089.7±30	1365.0
Pressurizer spray valve cycling ended	1246.0±0.1	1785.0
PORV cycling initiated	1467.9±0.1	1785.0
<b>L3-3</b>		
PORV latched open	3269.9±0.1	3295.1
Primary coolant pumps tripped off	3284.8±0.2	3295.1
Primary coolant pump coastdown completed	3304.2±0.8	3330.1
Upper plenum fluid reached saturation pressure	3329.4±0.2	3405.3
PORV closed	4849.7±0.1	4880.4
Steam generator secondary refill initiated	5114.6±0.2	5145.4
Natural circulation initiated	5205±10	-
Steam generator secondary refill completed	5746.4±0.2	6255.5
Pressurizer liquid level reached bottom of indicating range (0.06 m, above bottom)	5915±5	5570.5
Steam generator secondary feed-and-bleed initiated	6712.2±0.2	7230.4
Experiment completed	9517.4±0.2	-

#### 4.1.2 Long-term Responses

Most of the thermal-hydraulic phenomena during the long-term phase occurred following sub-sequences such as PCS pressure control by PORV cycling and latched open, plant recovery by refilling the SG secondary side, and removing decay heat through a feed-and-bleed operation using the secondary side.

Figure 8 presents a comparison of calculated and experimental pressure value during the long-term transient phase for both the PCS and SG secondary side. The cycling operation of the pressurizer spray valve controlled the PCS pressure from the 30 seconds. In the experiment, the pressurizer spray was closed by an operator at 1,246.0 seconds. For the RELAP5 model, the pressurizer spray was modeled to be terminated on the indication of the PORV actuation. As decay heat added to the PCS exceeded the cooling capability of the pressurizer spray, the PORV cycling operation started to regulate the PCS pressure. The PORV cycling operation continued for about 1,800 seconds until the PORV was latched open. During the cycling operation by both the pressurizer spray valve and the PORV, the pressure of the SG secondary side was decreased monotonously. Figure 8 shows that the code-predicted pressure behavior during this period matched very well with test data.

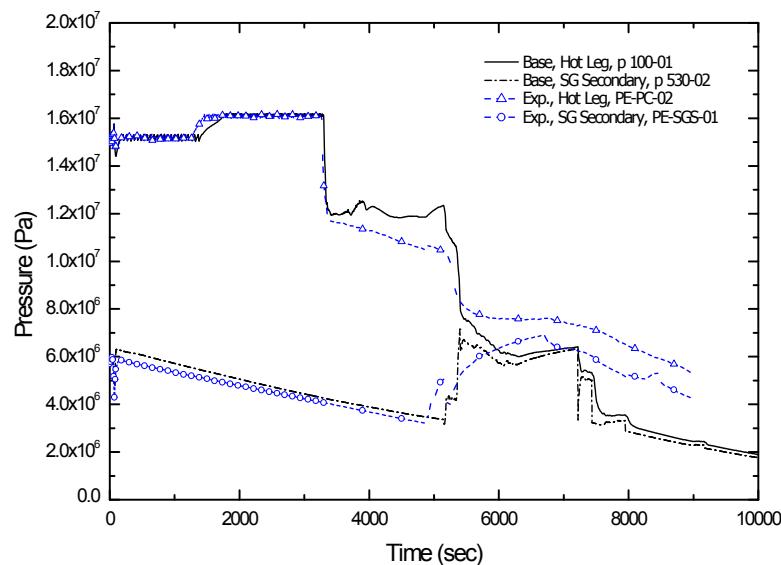


Figure 8. Comparison of Pressure for Long-term Response

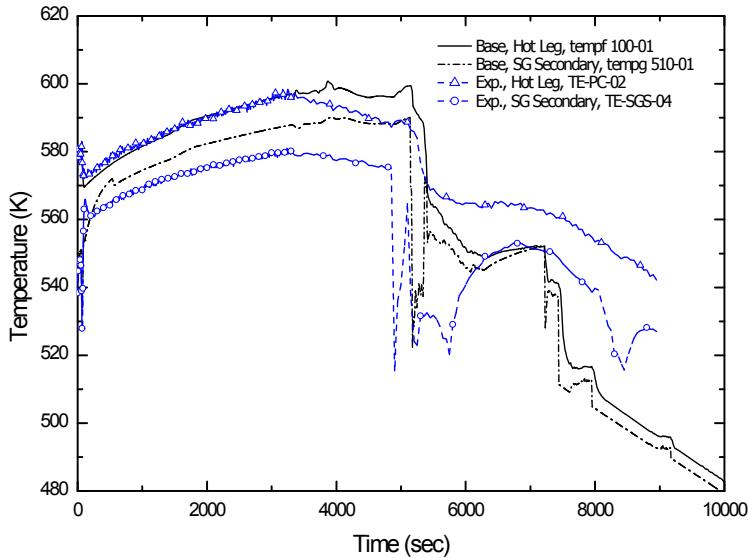


Figure 9. Comparison of Temperature for Long-term Response

The temperature for both the PCS and the SG secondary side during the cycling operation of the pressurizer spray valve and the PORV was increased gradually as presented in Figure 9. The calculated temperature of the PCS was in agreement with test data. The temperature of the SG secondary side, however, was over-estimated by the code. Since the SG was still in a de-coupled state from the PCS, the conservative prediction of the PCS behavior was not considered to be significant.

Figure 10 shows a comparison of pressurizer collapsed liquid level. It appears that the code-calculated liquid level is higher than the level in the experiment, especially during the PORV cycling operation. However, the difference is believed to be due to the fact that the differential pressure detector for water level calculation could not measure the water level over the upper detector location (1.83m, above bottom), while the code calculated the water level at the top of the pressurizer (2.0m, above bottom).

Experiment L3-3 was initiated by the PORV latched open. The LOFT plant recovery during this experiment was by two subsequent recovery procedures. The first recovery procedure was the PORV latched open to depressurize the primary coolant system. The second recovery procedure was by refilling the SG and removing decay heat through a feed-and-bleed operation using the SG secondary side.

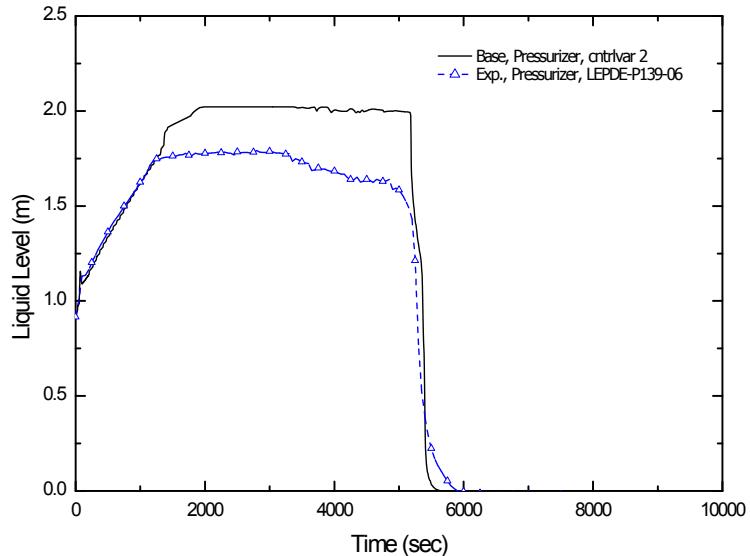


Figure 10. Comparison of Pressurizer Collapsed Liquid Level

The PORV was latched open at the 3,269.9 seconds, and maintained its state to 4849.7 seconds. The PCS pressure and temperature during the PORV latched open period was over-estimated by the code as seen in Figures 8 and 9, respectively. One of the reasons for this discrepancy was that the code-predicted excessive swelling of the PCS fluid during the time the PORV was latched open as noted in the reference calculation [4]. The excessive swelling of the code prediction can be confirmed from the behavior of the pressurizer water level in Figure 10.

The predicted water level during this period remained nearly constant, while the measured level decreased gradually as the fluid discharged through the PORV. This implies that the top of the pressurizer was filled with lower steam quality in the code calculation than in the experiment. Considering that water has much lower enthalpy than steam, the total discharged energy through the PORV would be under-estimated in the code, while the code-predicted mass flow rate through the PORV agreed well with the test data as shown in Figure 11. Therefore, it is concluded that over-estimation of the PCS pressure and temperature during the PORV latched open period is due to the code's under-estimation of total discharged energy through the PORV.

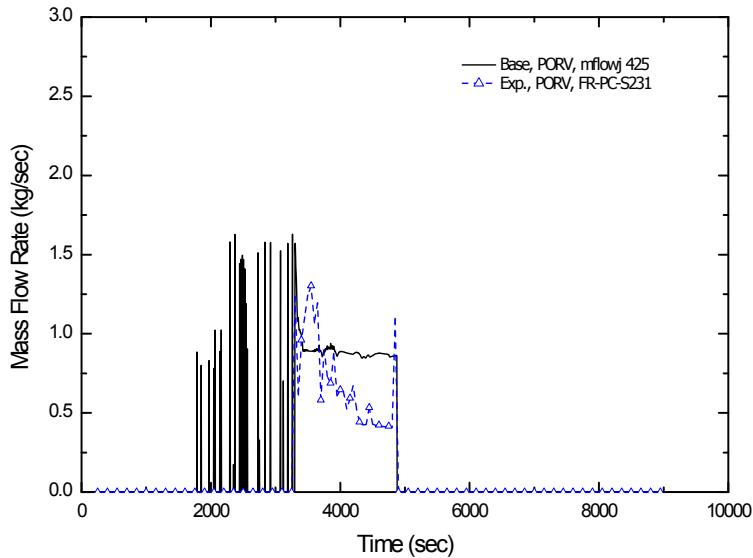


Figure 11. Mass Flow Rate through PORV for Long-term Response

Other important phenomena occurring during the period when the PORV was latched open were the changes in the fluid condition and the mass of the PCS. Figure 12 shows that the PCS fluid rapidly reached saturation conditions when the PORV was latched open, and, as a result, the steam started to be generated. In Figure 13, the change to the PCS system mass during this period is presented. It is apparent from Figure 13 that the code-calculated PCS mass behavior such as the total mass and the decreasing slope were very close to the measured data.

The second recovery procedure was initiated by refilling the SG secondary side through the auxiliary feedwater line, and the plant recovery was completed through feed-and-bleed operation. As the PCS was coupled again with the SG secondary side during the second recovery period, the PCS pressure and temperature decreased rapidly. It can be seen from Figures 8 and 9 that the code-predicted trends of the system pressure and temperature generally agree well with the experimental data, even though the excessive cooling by the code was also shown.

For the code-predicted excessive cooling during the second recovery procedure, the code modeling deficiency of the SG secondary side was presumed to be one of the reasons. However, the specific reasons for the deviation were not clearly identified in this assessment. Therefore, further investigations into the deviation sources are needed to enhance the code's predictability.

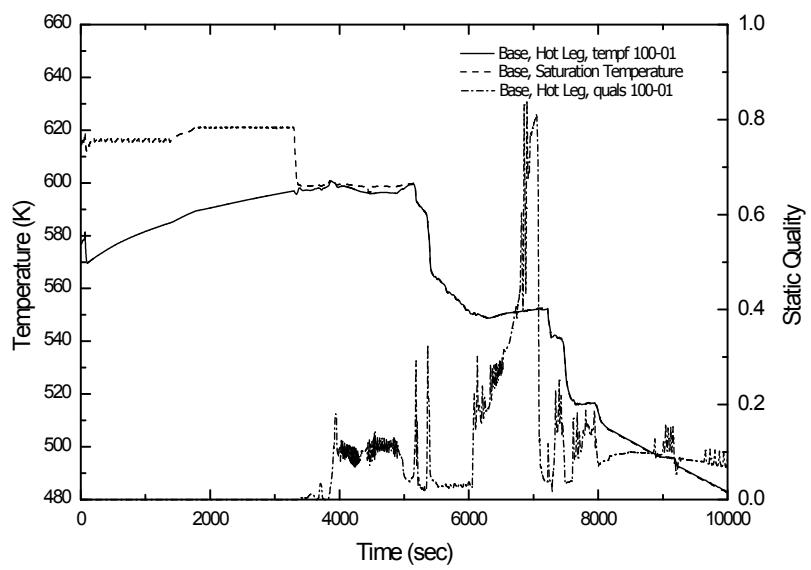


Figure 12. Fluid Conditions of Hot Leg for Long-term Response

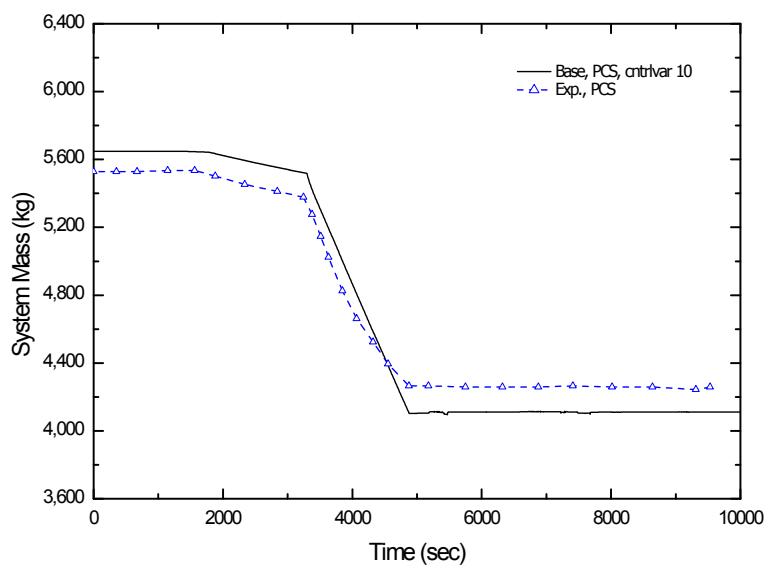


Figure 13. System Mass of PCS for Long-term Response

## 4.2 Sensitivity Studies

The sensitivity studies were performed to identify parameters having significant effect on the predicted thermal hydraulic behaviors. The cases and the parameters for the sensitivity studies are presented in Table 3. The first three parameters were selected as short-term parameters, while the last two were chosen as parameters which affect the long-term transient behavior. The code-predicted results for each case are compared with both the base calculation and the experimental data in Figures 14 through 17.

Table 3. Matrix for Sensitivity Studies

PARAMETERS \ CASES		Base	Case 1	Case 2	Case 3	Case 4	Case 5
Short-term Parameters	Pressurizer Spray Valve Loss Coefficient	1.0	15.432 (Note 1)	Base	Base	Base	Base
	SG Nodalization	6	Base	3 (Note 1)	Base	Base	Base
	SG U-tube Heat Trans. Area (Cylinder Height)	12149.9 m <sup>2</sup>	Base	Base	10124.9 m <sup>2</sup> (Note 1)	Base	Base
Long-term Parameters	Heat Transfer Coefficient to Environment	(Note 2)	Base	Base	Base	(Note 1)	Base
	PORV Discharge Coefficient	0.8	Base	Base	Base	Base	1.0 (Note 1)

Notes:

1. These values are identical to those in NUREG/IA-0114 [4]. The environmental loss heat transfer coefficients for components are as follows:  
Reactor Vessel and Pipe: 13.450 W/m<sup>2</sup>K  
Steam Generator: 3.385 W/m<sup>2</sup>K  
Pressurizer: 3.019 W/m<sup>2</sup>K
2. Compared to those in the NUREG/IA-0114, the environmental loss heat transfer coefficients for these cases are increased by 40% as follows:  
Reactor Vessel and Pipe: 18.830 W/m<sup>2</sup>K  
Steam Generator: 4.739 W/m<sup>2</sup>K  
Pressurizer: 4.227 W/m<sup>2</sup>K

### 4.2.1 Pressurizer Spray System Loss Coefficient (Case 1)

The pressurizer spray in the LOFT facility was used to regulate the PCS pressure by condensing steam at the top of the pressurizer. The loss coefficient of the pressurizer spray system which determines the amount of the spray flow was known to have a remarkable effect on the RCS pressure behavior [9]. In this sensitivity study, the effect of the mass flow rate

through the spray valve was investigated. The mass flow rate was reduced from 1.7 kg/sec to 1.0 kg/sec by increasing the loss coefficient of the spray valve from 1.0 to 15.432 [4]. From the comparison in Figure 14, it is seen that the pressure before reactor scram increased more rapidly than for the base calculation, as the reduced mass flow rate was not sufficient to suppress the pressure increase. The pressure increase after the reactor scram, however, was slower than that for the base calculation because the heat added to the PCS was smaller than in the base calculation due to the earlier reactor trip.

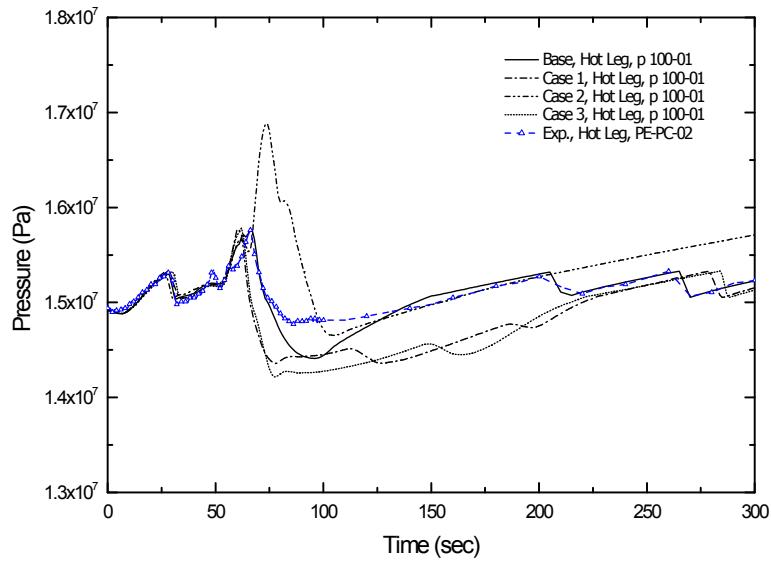


Figure 14. Sensitivity Studies for Short-term Parameters

#### 4.2.2 Steam Generator Nodalization (Case 2)

The heat transfer phenomena through the SG U-tube plays a very important role in this type of transient, because the heat generated in the reactor is mainly removed by the SG secondary side until it is de-coupled after a complete depletion. The SG nodalization is one of the most important parameters which affect the heat transfer phenomena through the SG [9, 10]. The effect of coarse nodalization of the SG was examined for this case. The nodes of the SG U-tube and the SG secondary side associated with the U-tube were reduced from 6 to 3 nodes, which implied that the subdivided four nodes in the base calculation were merged into one node as in the reference calculation [4]. As shown in Figure 14, this modeling change caused completely different results from the base calculation. The PCS pressure surge was not controlled, even though the reactor trip was accomplished on indication of the PCS high pressure. The pressure was not suppressed until it had increased sharply to the PORV actuation set pressure. The reason for this can be deduced from a comparison of the heat transfer rate through the U-tube.

Figure 15 shows that the heat transfer rate during the period of the steep pressure increase after the reactor trip was lower for this case than for the base calculation, which led to the PCS over-pressurization. Therefore, the PCS over-pressurization can be attributed to the coarse nodalization of the SG U-tube and the associated SG secondary side.

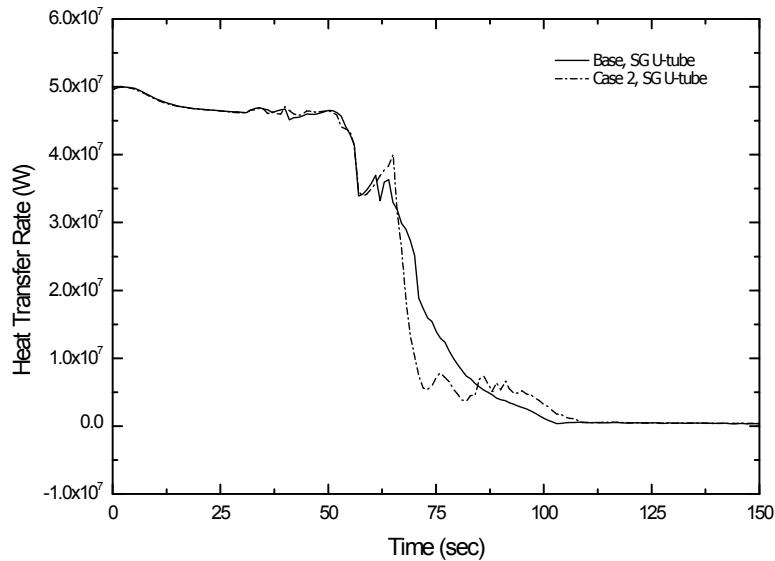


Figure 15. Comparison of Heat Transfer Rate through SG U-tube

#### 4.2.3 Steam Generator U-tube Heat Transfer Area (Case 3)

The heat transfer area of the SG U-tube was generally identified as a factor to have an impact on the initial conditions in the SG secondary side [4, 11]. This implies that the SG U-tube heat transfer area may also affect the SG heat transfer phenomena during the transient phase. Therefore, the SG U-tube heat transfer area also selected as a sensitivity parameter. In this sensitivity study, the heat transfer area of all the nodes of the SG U-tube was reduced to  $10,124.886 \text{ m}^2$  [4] from  $12,149.864 \text{ m}^2$  in the base calculation. From Figure 14, the PCS pressure behavior for Case 3 is very similar to that in the Case 1, i.e., reduction of the pressurizer spray valve loss coefficient. The reactor tripped earlier due to the reduced heat transfer to the SG secondary side, and the pressure increase after the reactor trip was slower than for the base calculation due to the reduced heat added to the PCS from the reactor core as in Case 1.

#### 4.2.4 Heat Transfer Coefficient to Environment (Case 4)

Generally, the heat losses to the environment from the plant main components after a reactor trip can affect the long-term trend of the transient since the amount of the heat loss to the environment is not negligible compared to the decay heat level. In the previous calculation using RELAP5/MOD1, the PCS fluid heatup rate during the PORV cycling operation was much faster than in the experiment, and the amount of the discharged coolant through the PORV was greater in the calculation than in the experiment [3, 7]. This difference was considered due to higher environmental heat losses from the primary system than assumed [3]. In this sensitivity study, the effect of the environmental heat loses was investigated. The values from reference calculation [4] were used as heat transfer coefficients of the major components such as the

reactor vessel, the steam generator, the pressurizer, and primary coolant system, as shown in Table 3. This implies that the total heat loss to the environment from the plant main components was decreased by about 40% in this sensitivity study. As shown in Figure 16, the environmental heat loss mainly affected the PCS temperature behavior during the cycling operation period of both the pressurizer spray and the PORV. During this period, the temperature increased more rapidly than for the base calculation as the total heat loss to the environment was reduced. In addition, the steeper temperature increase resulted in the successive key events such as the PORV latched open, the SG refill, and the feed-and-bleed operation to occur earlier than for the base calculation.

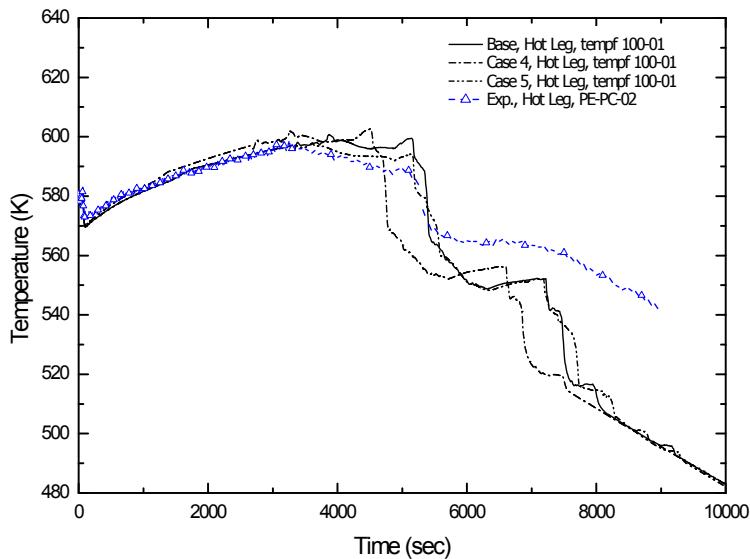


Figure 16. Sensitivity Studies for Long-term Parameters

#### 4.2.5 PORV Discharge Coefficient (Case 5)

The effect of the discharge coefficient and the thermal nonequilibrium constant of the PORV were checked by setting them at 1.0 and 0.14, respectively. The calculated mass flow rates using these setting are compared in Figure 17. Compared to the base calculation, the mass flow rate through the PORV for this sensitivity increased up to 50% during the PORV latched open period as shown in Figure 17. This increased mass flow resulted in a more rapid PCS cooling during the PORV latched open period. However, the PCS temperature behavior during the cycling operation of the PORV was not influenced by the increased mass flow rate through the PORV as shown in Figure 16.

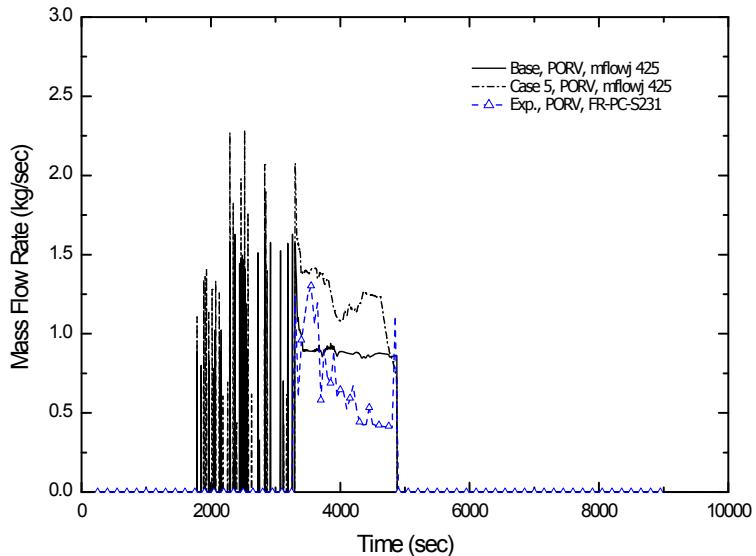


Figure 17. Sensitivity Study for Mass Flow Rate through PORV

#### 4.3 Run Statistics

An IBM Personal Computer (Pentium III 933 MHz) was used for the present calculations with a DOS operating system. The required CPU time and the time step size with respect to the real transient times for the base calculation are presented in Figures 18 and 19, respectively. Figure 18 shows that the required CPU time up to the real transient time of 10,000 seconds is 2,427.76 seconds, including the input processing time of 3.46 seconds. Therefore, the grind time for the base calculation is calculated as follows:

$$\text{CPU time, } \quad \text{CPU} = 2,427.76 - 3.46 = 2424.3 \text{ sec}$$

$$\text{Number of time steps, DT} = 125,092$$

$$\text{Number of volumes, C} = 134$$

$$\text{Grind time} = \text{CPU} \times 1,000 / (\text{C} \times \text{DT}) = 0.14463 \text{ CPU msec/vol/step}$$

In Figure 19, the advanced time step size is compared with the Courant time step size. The maximum time steps specified in the base input decks were 1.0 second up to 1,000 seconds, 0.1 second up to 2,000 seconds, 0.5 second up to 4,000 seconds, 0.1 second up to 8,000 seconds, and 0.5 second up to 10,000 seconds of the real transient time. It is shown in Figure 19 that the advanced time step sizes were below the Courant time step sizes throughout the transient.

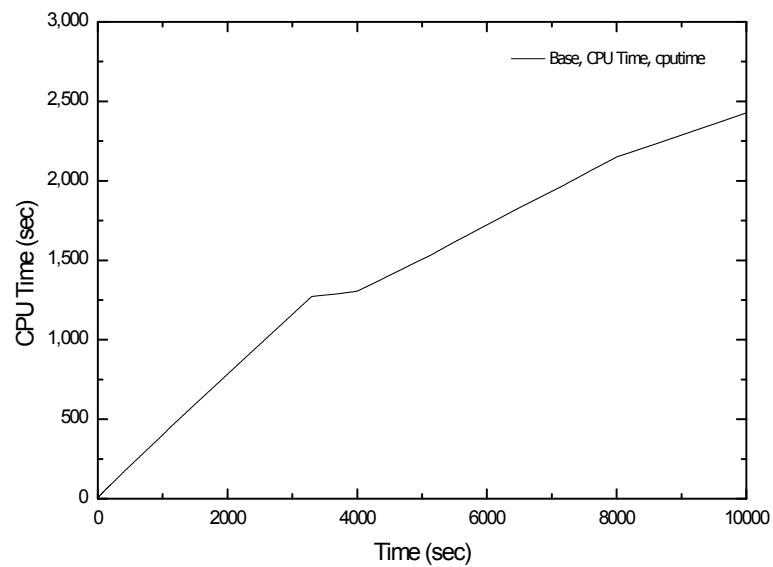


Figure 18. Required CPU Time of Base Calculation

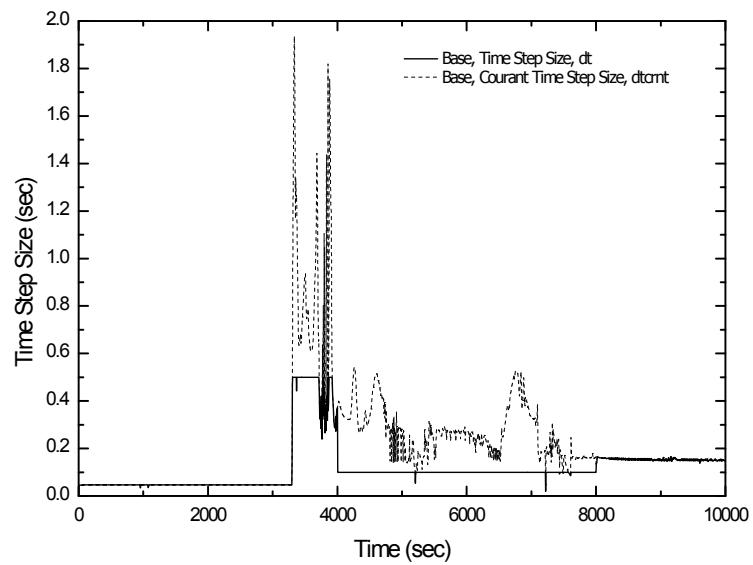


Figure 19. Time Step Size of Base Calculation

## **5. CONCLUSIONS**

The purpose of this report is to assess the capability of the RELAP5/MOD3.3Beta computer code to simulate thermal-hydraulic behavior associated with the LOFT Experiment L9-1/L3-3. For this purpose, major parameters identified through sensitivity studies to have the most significant effect on the predicted thermal-hydraulic behaviors were incorporated into the base calculation to improve the code predictability. The code-predicted results were compared with the experimental data to assess the code predictability. Major conclusions through this assessment are summarized as follows:

From the comparisons presented with Figures and Tables, it was shown that the code-predicted results were generally in agreement with the measured data. Therefore, it is concluded that the RELAP5/MOD3.3Beta computer code has sufficient capability in predicting the thermal hydraulic phenomena occurred in the LOFT Experiment L9-1/L3-3.

However, the discrepancies between the calculation and the experiment were also identified. In Experiment L9-1, the code over-estimated temperature behaviors of the SG secondary side after dryout of the SG. However, these discrepancies were not considered to be significant, since the SG was in a de-coupled state from the PCS after the dryout of the SG secondary side. In Experiment L3-3, the code predicted excessive swelling of the PCS fluid during the first recovery mode, and predicted excessive cooling during the second recovery mode. The differences during the first recovery mode were due to the code's under-estimation of total discharged energy through the PORV. For the discrepancies during the second recovery mode, the code modeling deficiency of the SG secondary side was presumed to be one of the reasons. However, it is concluded that further investigation into the deviation sources are needed to enhance the code's predictability, since the specific reasons for the deviation were not clearly identified in this assessment.

Through sensitivity studies, the major parameters were identified to have significant effect on the predicted thermal-hydraulic behaviors. These parameters include the pressurizer spray system loss coefficient, nodalization of the SG secondary side, SG U-tube heat transfer area, heat transfer coefficient from the LOFT main components to the environment, and the PORV discharge coefficient. The first three parameters are significant during the short-term transient phase, while the last two are significant during the long-term transient phase. Therefore, the five parameters listed above should be carefully modeled to obtain appropriate calculation results for transient types such as the total-loss-of feedwater accident and its recovery modes.



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## **Appendix A**

### **Steady State Input Deck for Base Case**



```

=loft l9-1 post test analysis deck
*----1---1---1---1---1---1---1---1---1---
*      initial conditions
*
*      core power = 50. mw
*      pcs flow = 479.3 kg/s
*      thot = 578. k
*      tcold = 559.0 k
*
*----1---1---1---1---1---1---1---1---
0000100 new stdy-st
0000101 run
0000102 si
0000105 5. 10.
0000110 nitrogen
* time step control cards
*      end time min dt  max dt otn mnr mjr rst
0000201 1000.0 1.e-6 0.5   3   4   500 200
***** minor edit variables
*****
* pressure
*****
0000301 p    345010000 * pe-bl-1
0000302 p    310010000 * pe-bl-2
0000303 p    315110000 * pe-bl-3
0000304 p    350010000 * pe-bl-4
0000305 p    315090000 * pe-bl-6
0000306 p    350020000 * pe-bl-8
0000307 p    185010000 * pe-pc-1
0000308 p    100010000 * pe-pc-2
0000309 p    420010000 * porv inlet
0000310 p    110010000 * pt-139-2,3,4
0000311 p    245010000 * pe-1up-1a,1b
0000312 p    215010000 * pe-1st-1a,b/pe-2st-1a,b
0000313 p    200010000 * pe-1st-3a,3b
0000314 p    530020000 * pt-p4-10a
0000315 p    535010000 * pt-p4-85
*****
* temperatures
*****
0000320 tempf 406010000 * spray tempf
0000321 tempf 310010000 * te-bl-2a,2b,2c
0000322 tempf 100010000 * te-pc-2a,2b,2c
0000323 tempf 185010000 * te-pc-1
0000324 tempf 115030000 * te-sg-1
0000325 tempf 115100000 * te-sg-2
0000326 tempf 515040000 * te-sg-3
0000328 tempf 415050000 * pqr volume 5
0000329 tempf 415040000 * te-139-19
0000330 tempf 415030000 * te-139-20
0000331 tempf 315120000 * te-p138-171
0000332 tempf 350020000 * te-p138-170
0000333 tempf 205010000 * te-1st-1/te-2st-1
0000334 tempf 210010000 * te-1st-2/te-2st-2
0000335 tempf 345010000 * te-bl-1
0000336 tempf 210030000 * te-1st-14/te-2st-14
0000337 tempf 210040000 * te-3up-2
0000338 tempf 245010000 * te-1up-6
0000339 tempf 246010000 * te-2up-4
0000340 tempf 250010000 * te-1up-3
*****
* densities
*****
0000341 rho   345010000 * de-bl-1
0000342 rho   310010000 * de-bl-2
0000343 rho   185010000 * de-pc-1
0000344 rho   100010000 * de-pc-2
0000345 rho   115120000 * de-pc-3
0000346 voidgj 400010000 * surge line density
0000347 rho   115040000 * s/g tubes
0000348 rho   115050000 * s/g tubes
0000349 rho   115060000 * s/g tubes
0000350 rho   115070000 * s/g tubes
*****
* velocities
*****
0000351 voidf 100010000 * ihl nozzle
0000352 velf 100010000 * ihl nozzle
0000353 velf 115030000 * s/g inlet
0000354 velf 400010000 * surge line
0000355 velfj 425000000 * porv liq vel
0000356 velg 100010000 * ihl nozzle
0000357 velg 115030000 * s/g inlet
0000358 velg 400010000 * surge line
0000359 velgj 425000000 * porv vap vel
*****
* mass flow rates
*****
0000360 mflowj 100010000 * ihl nozzle
0000361 mflowj 150010000 * pump outlet
0000362 mflowj 185020000 * dtt-rake ilcl
0000363 mflowj 400010000 * pres. surge line flow
0000364 mflowj 407000000 * pqr spray flow
0000366 mflowj 425000000 * pres. relief valve flow
0000367 mflowj 550000000 * steam flow control valve
0000368 mflowj 548000000 * aux feed
0000369 mflowj 560000000 * main feed
0000370 cntrvar 1       * s/g level
*****
* cladding temperatures center module
*****
0000371 httemp 230000110 * te-5h-015
0000372 httemp 230000210 * te-5h-034
0000373 httemp 230000310 * te-5h-049
*****
* peak centerline temperatures
*****
0000374 httemp 230000101 * core lower region
0000375 httemp 230000201 * core middle region
0000376 httemp 230000301 * core upper region
*****
* reactor kinetic parameters
*****
0000377 rktpow 0         * total reactor power
0000378 rkfpow 0         * fission decay power
0000379 rkgapow 0        * gamma decay power
0000380 rkreac 0         * reactivity

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0000381	ppmhead	135	* pcp1 head		0000570	p	420010000	gt null	0	1.620058e7	n		
0000382	ppmhead	165	* pcp2 head		0000571	p	420010000	lt null	0	1.606269e7	n		
0000384	cntrlvar	2	* pqr level		0000572	p	420010000	lt null	0	1.486300e7	n		
0000385	cntrlvar	3	* rx vessel level		0000573	p	420010000	gt null	0	1.506980e7	n		
0000386	mflowj	185010000			0000574	p	420010000	gt null	0	1.533874e7	n		
0000387	mflowj	185030000			0000575	p	420010000	lt null	0	1.505000e7	n		
0000388	mflowj	200020000			0000576	p	420010000	lt null	0	1.482853e7	n		
0000389	ppmvel	135			0000577	p	420010000	gt null	0	1.495950e7	n		
0000390	ppmvel	165			*****								
***** logical trips *****													
*					0000600	670							
*					0000601	563	and	561	n				
*					0000602	-563	and	-564	n				
*					0000603	655	and	602	n				
*					0000604	609	or	609	l				
*					0000605	572	and	-509	n				
*					0000606	-572	and	-573	n				
*					0000607	608	and	606	n				
*					0000608	605	or	607	n				
*					0000609	504	or	504	l				
*					0000610	612	or	520	n				
*					0000611	-521	and	-616	n				
*					0000612	611	and	610	n				
*					0000613	616	or	523	n				
*					0000614	-522	and	613	n				
*					0000615	-612	and	609	n				
*					0000616	615	and	614	n				
*					0000617	612	or	616	n				
*					0000618	605	or	607	n				
*					0000621	623	or	570	n				
*					0000622	-571	and	-571	n				
*					0000623	621	and	622	n				
*					0000624	509	and	-552	n				
*					0000625	623	or	624	n				
*					0000626	576	and	-509	n				
*					0000627	-576	and	-577	n				
*					0000628	629	and	627	n				
*					0000629	626	or	628	n				
*					0000635	504	and	504	n				
*					0000636	509	and	-536	n				
*					0000650	-652	and	550	n				
0000520	p	530020000	gt null	0	7.103448e6	n	0000651	650	or	652	n		
0000521	p	530020000	lt null	0	7.0344827e6	n	0000652	-509	and	651	n		
0000522	p	530020000	gt null	0	6.3448275e6	n	0000655	601	or	603	n		
0000523	p	530020000	lt null	0	6.4137931e6	n	0000656	508	or	609	n		
0000530	time	0	ge null	0	3600.0	n	0000659	561	or	562	n		
0000531	p	530020000	gt p	547010000.0	0.0	n	0000660	504	or	504	n		
0000536	time	0	ge null	0	10000.0	n	0000669	561	and	564	l		
0000540	tempf	100010000	gt null	0	583.16	l	0000670	565	and	-655	n		
0000541	p	100010000	gt null	0	1.574553e7	l	0000680	530	or	530	n		
0000550	time	0	ge null	0	10000.0	l	0000688	690	or	574	n		
0000551	time	0	ge timeof	625	0.0	l	0000689	-575	and	-551	n		
0000552	time	0	ge timeof	509	1580.	l	0000690	688	and	689	n		
0000560	p	100010000	le null	0	13.15862e6	n	*****						
0000561	time	0	ge timeof	552	265.0	l	*						
0000562	time	0	gt null	0	5400.0	n	*						
0000563	cntrlvar	1	lt null	0	2.1844	n	*						
0000564	cntrlvar	1	gt null	0	2.9464	n	*****						
0000565	time	0	ge timeof	669	966.	l	*						
* reactor vessel nozzle - intact loop hot leg													

*****							1150405	0.335	16
1000000	rvnilhl	branch					1150406	0.0437	17
1000001	2	0					1150407	0.0462	18
1000101	0.0634	1.5373	0.0	0.0	0.0	0.0	1150408	0.0	19
1000102	4.0e-5	0.0	00000				1150501	0.0	19
1000200	0	14901000.	1346300.0	2462060.0	0.0		1150601	0.0	1
1001101	250000000	100000000	0.0634	0.0	0.0	000100	1150602	90.0	9
1002101	100010000	105000000	0.0	0.05	0.05	000100	1150603	-90.0	19
1001201	10.582000	11.005000	0.0				1150701	0.0	1
1002201	10.582000	10.625000	0.0				1150702	0.246	2
*****							1150703	0.513	3
* pressurizer connection tee reactor vessel side							1150704	0.26675	7
*****							1150705	1.067	8
1050000	pzrtrs	branch					1150706	0.2865	9
1050001	1	0					1150707	-0.2865	10
1050101	0.0634	1.634	0.0	0.0	0.0	0.0	1150709	-1.067	11
1050102	4.0e-5	0.0	00000				1150710	-0.26675	15
1050200	0	14896100.	1346300.	2462190.0	0.0		1150711	-0.513	16
1051101	105010000	110000000	0.0	0.05	0.05	000100	1150712	-0.498	17
1051201	13.795000	13.974000	0.0				1150713	-0.689	18
*****							1150714	-0.356	19
* steam generator inlet piping							1150801	4.0e-5	0.0
*****							1150802	4.0e-5	0.0102
1100000	sginlp	branch					1150803	1.0e-5	0.0103
1100001	1	0					1150804	4.0e-5	0.0102
1100101	0.0	0.623	0.0303	0.0	0.0	0.0	1150805	4.0e-5	0.0
1100102	4.0e-5	0.0	00000				1150901	0.15	0.15
1100200	0	14857200.	1346340.	24629400.0	0.0000000		1150902	0.05	0.05
1101101	110010000	115000000	0.0	0.1	0.1	000100	1150903	0.0	0.0
1101201	13.801000	13.692000	0.0				1150904	0.1	0.1
*****							1150905	0.2	0.2
* steam generator plus piping							1150906	0.1	0.1
*****							1150907	0.0	0.0
1150000	sgppip	pipe					1150908	0.05	0.05
1150001	19						1150909	0.1	0.1
1150101	0.0	3					1151001	00000	19
1150102	0.151	15					1151101	000100	2
1150103	0.0	18					1151102	100100	3
1150104	0.0634	19					1151103	000000	14
1150201	0.0	1					1151104	000100	18
1150202	0.0512	2					1151201	0	14871600. 1346350.
1150203	0.0	15					1151202	0	14877200. 1346350.
1150204	0.0512	16					1151203	0	14793300. 1346370.
1150205	0.0	18					1151204	0	14770000. 1321980.
1150301	1.4385	1					1151205	0	14746400. 1301720.
1150302	0.708	2					1151206	0	14729700. 1283950.
1150303	0.63	3					1151207	0	14721700. 1268380.
1150304	0.26675	7					1151208	0	14715000. 1254890.
1150305	1.067	8					1151209	0	14707300. 1242570.
1150306	0.45	10					1151210	0	14707600. 1242600.
1150307	1.067	11					1151211	0	14631100. 1242600.
1150308	0.26675	15					1151212	0	14621800. 1242600.
1150309	0.63	16					1151213	0	14616700. 1242600.
1150310	0.547	17					1151300	0	14681000. 0.0
1150311	0.689	18					1151301	10.728000	10.670000
1150312	0.559	19					1151302	8.3370000	8.4284000
1150401	0.09	1					1151303	4.4456000	4.7693000
1150402	0.057	2					1151304	4.3865000	4.2164000
1150403	0.335	3					1151305	4.3407000	4.6700000
1150404	0.0	15					1151306	4.3009000	4.6296000





1353001	0.000000e+00	0.000000e+00		1354308	-2.500000e-01	-1.690000e+00
1353002	2.000000e-02	2.000000e-02		1354309	-1.000000e-01	-5.000000e-01
1353003	6.000000e-02	5.000000e-02		1354310	0.000000e+00	0.000000e+00
1353004	1.000000e-01	1.000000e-01	*----1---1---1---1---1---1---1---			
1353005	2.000000e-01	4.600000e-01	*----1---1---1---1---1---1---1---			
1353006	2.400000e-01	8.000000e-01	*----1---1---1---1---1---1---1---			
1353007	3.000000e-01	9.600000e-01		1354400	1	4
1353008	4.000000e-01	9.800000e-01		1354401	-1.000000e+00	-1.160000e+00
1353009	6.000000e-01	9.700000e-01		1354402	-9.000000e-01	-7.800000e-01
1353010	8.000000e-01	9.000000e-01		1354403	-8.000000e-01	-5.000000e-01
1353011	9.000000e-01	8.000000e-01		1354404	-7.000000e-01	-3.100000e-01
1353012	9.600000e-01	5.000000e-01		1354405	-6.000000e-01	-1.700000e-01
1353013	1.000000e+00	0.000000e+00		1354406	-5.000000e-01	-8.000000e-02
*----1---1---1---1---1---1---1---				1354407	-3.500000e-01	0.000000e+00
* torque curve				1354408	-2.000000e-01	5.000000e-02
*----1---1---1---1---1---1---1---				1354409	-1.000000e-01	8.000000e-02
1353100	0			1354410	0.000000e+00	1.100000e-01
1353101	0.000000e+00	0.000000e+00		*----1---1---1---1---1---1---1---		
1353102	1.250000e-01	7.000000e-02		* head curve no. 5		
1353103	1.650000e-01	1.250000e-01		*----1---1---1---1---1---1---1---		
1353104	2.400000e-01	5.600000e-01		1354500	1	5
1353105	8.000000e-01	5.600000e-01		1354501	0.000000e+00	0.000000e+00
1353106	9.600000e-01	4.500000e-01		1354502	2.000000e-01	-3.400000e-01
1353107	1.000000e+00	0.000000e+00		1354503	4.000000e-01	-6.500000e-01
******				1354504	6.000000e-01	-9.300000e-01
* pump 2-phase difference data				1354505	8.000000e-01	-1.190000e+00
******				1354506	1.000000e+00	-1.470000e+00
* head curve no. 1				*----1---1---1---1---1---1---1---		
*----1---1---1---1---1---1---1---				* head curve no. 6		
1354100	1	1		*----1---1---1---1---1---1---1---		
1354101	0.000000e+00	0.000000e+00		1354600	1	6
1354102	1.000000e-01	8.300000e-01		1354601	0.000000e+00	1.100000e-01
1354103	2.000000e-01	1.090000e+00		1354602	1.000000e-01	1.300000e-01
1354104	5.000000e-01	1.020000e+00		1354603	2.500000e-01	1.500000e-01
1354105	7.000000e-01	1.010000e+00		1354604	4.000000e-01	1.300000e-01
1354106	9.000000e-01	9.400000e-01		1354605	5.000000e-01	7.000000e-02
1354107	1.000000e+00	1.000000e+00		1354606	6.000000e-01	-4.000000e-02
*----1---1---1---1---1---1---1---				1354607	7.000000e-01	-2.300000e-01
* head curve no. 2				1354608	8.000000e-01	-5.100000e-01
*----1---1---1---1---1---1---1---				1354609	9.000000e-01	-9.100000e-01
1354200	1	2		1354610	1.000000e+00	-1.470000e+00
1354201	0.000000e+00	0.000000e+00		*----1---1---1---1---1---1---1---		
1354202	1.000000e-01	-4.000000e-02		* head curve no. 7		
1354203	2.000000e-01	0.000000e+00		*----1---1---1---1---1---1---1---		
1354204	3.000000e-01	1.000000e-01		1354700	1	7
1354205	4.000000e-01	2.100000e-01		1354701	-1.000000e+00	0.000000e+00
1354206	8.000000e-01	6.700000e-01		1354702	0.000000e+00	0.000000e+00
1354207	9.000000e-01	8.000000e-01		*----1---1---1---1---1---1---1---		
1354208	1.000000e+00	1.000000e+00		* head curve no. 8		
*----1---1---1---1---1---1---1---				*----1---1---1---1---1---1---1---		
* head curve no. 3				1354800	1	8
*----1---1---1---1---1---1---1---				1354801	-1.000000e+00	0.000000e+00
1354300	1	3		1354802	0.000000e+00	0.000000e+00
1354301	-1.000000e+00	-1.160000e+00		*----1---1---1---1---1---1---1---		
1354302	-9.000000e-01	-1.240000e+00		* torque curve no. 1		
1354303	-8.000000e-01	-1.770000e+00		*----1---1---1---1---1---1---1---		
1354304	-7.000000e-01	-2.360000e+00		1354900	2	1
1354305	-6.000000e-01	-2.790000e+00		1354901	0.000000e+00	6.032000e-01
1354306	-5.000000e-01	-2.910000e+00		1354902	1.930000e-01	6.325000e-01
1354307	-4.000000e-01	-2.670000e+00		1354903	3.930000e-01	7.369000e-01







2351202	0	15002400.	1242980.	2459850.0	0.0	0.0	02		3002101	300010000	305000000	0.0	0.1	0.1	000000	
2351203	0	14981700.	1243020.	2460330.0	0.0	0.0	03		3001201	-1303100	-1795200	0.0				
2351300	0								3002201	-1303200	-1304000	0.0				
2351301	2.2307000	2.3978000	0.0	01					*----1----	--1----	--1----	--1----	--1----	--1----		
2351302	2.2307000	2.3980000	0.0	02					* hot leg pipe to reflood assist bypass tee							
*----1----	--1----	--1----	--1----	--1----					*----1----	--1----	--1----	--1----	--1----	--1----		
* upper core support structure									3050000	hlpras	branch					
*----1----	--1----	--1----	--1----	--1----					3050001	1	0					
2400000	ucosst	branch							3050101	0.0634	0.698	0.0	0.0	0.0	0.0	
2400001	2	0							3050102	4.0e-5	0.0	00000				
2400101	0.297	1.118	0.0	0.0	90.0	1.118			3050200	0	14953100.	1239750.	2460990.0	0.0		
2400102	4.0e-5	0.145	00000						3051101	305010000	310000000	0.0	0.1	0.1	000100	
2400200	0	14966500.	1348980.	2460680.0	0.0				3051201	-1.761300	-1768800	0.0				
2401101	230010000	240000000	0.12	0.3	0.3	000100			*----1----	--1----	--1----	--1----	--1----	--1----		
2402101	235010000	240000000	0.0	0.0	0.0	000100			* broken loop hot leg contraction							
2401201	3.6456000	3.6509000	0.0						*----1----	--1----	--1----	--1----	--1----	--1----		
2402201	2.3080000	2.3981000	0.0						3100000	sgsii	branch					
*----1----	--1----	--1----	--1----	--1----					3100001	2	0					
* upper flow skirt region									3100101	0.0	1.424	0.0668	0.0	0.0	0.0	
*----1----	--1----	--1----	--1----	--1----					3100102	4.0e-5	0.0	00000				
2450000	ufosre	branch							3100200	0	14953100.	1239700.	2460990.0	0.0		
2450001	1	0							3101101	370010000	310000000	0.0	0.0	0.0	000100	
2450101	0.114	0.843	0.0	0.0	90.0	0.843			3102101	310010000	315000000	0.0	0.0	0.0	000100	
2450102	4.0e-5	0.131	00000						3101201	.21294000	.26136000	0.0				
2450200	0	14945200.	1347660.	2461140.0	0.0				3102201	.00000000	.00320000	0.0				
2451101	240010000	245000000	0.0	0.0	0.0	000100			*----1----	--1----	--1----	--1----	--1----	--1----		
2451201	5.7436	6.0742	0.0						* steam generator and pump simulator							
*----1----	--1----	--1----	--1----	--1----					*----1----	--1----	--1----	--1----	--1----	--1----		
* dead end of fuel modules									3150000	sgpsi	pipe					
*----1----	--1----	--1----	--1----	--1----					3150001	12						
2460000	fumodu	branch							3150101	0.00836	2					
2460001	1	0							3150102	0.108	8					
2460101	0.183	0.7	0.0	0.0	90.0	0.7			3150103	0.0	10					
2460102	4.0e-5	0.214	00000						3150104	0.00836	11					
2460200	0	14961800.	1343000.	2460790.	0.0				3150105	0.0525	12					
2461101	240010000	246000000	0.0	0.0	0.0	000100			3150201	0.0	2					
2461201	-.74932e-5	-.74932e-5	0.0						3150202	0.0326	4					
*----1----	--1----	--1----	--1----	--1----					3150203	0.108	5					
* upper plenum lower volume									3150204	0.0326	7					
*----1----	--1----	--1----	--1----	--1----					3150205	0.0	8					
2500000	uplvol	branch							3150206	0.0	9					
2500001	1	0							3150207	0.0081	10					
2500101	0.268	1.566	0.0	0.0	90.0	1.566			3150208	0.0	11					
2500102	4.0e-5	0.0	00000						3150301	0.4054	1					
2500200	0	14947600.	1346300.	2461140.0	0.0				3150302	0.5265	2					
2501101	245010000	250000000	0.0	0.0	0.0	000100			3150303	0.362	3					
2501201	5.8130000	6.1784000	0.0						3150304	1.692	4					
*****									3150305	0.8495	6					
*									3150306	1.692	7					
* broken loop									3150307	0.362	8					
*									3150308	1.346	9					
*****									3150309	1.325	10					
* reactor vessel nozzle - broken loop hot leg									3150310	1.842	11					
*----1----	--1----	--1----	--1----	--1----					3150311	0.667	12					
3000000	rvblhl	branch							3150401	0.0	8					
3000001	2	0							3150402	0.0162	9					
3000101	0.0634	0.876	0.0	0.0	0.0	0.0			3150403	0.0648	10					
3000102	4.0e-5	0.0	00000						3150404	0.0	12					
3000200	0	14953100.	1239820.	2460990.0	0.0				3150601	90.0	5					
3001101	250000000	300000000	0.0634	0.0	0.0	000100			3150602	-90.0	10					



3500201	0.0	1	* break plane		3770101	380010000	375000000	0.0	1.4e+4	1.4e+4
3500301	0.488	1			000000					
3500302	1.6085	2			3770201	0	.106460	.25646	0.0	
3500401	0.00541	1			*----1---1---1---1---1---1---1---					
3500402	0.07770	2			* reflood assist bypass parrel pipes cold leg side					
3500601	0.0	2			*----1---1---1---1---1---1---1---					
3500801	4.0e-5	0.0	1		3800000	rabppcl	snglvol			
3500802	4.0e-5	0.0	2		3800101	0.0776	0.0	0.0855	0.0	0.0
3500901	0.0	0.0	1		3800102	4.0e-5	0.0	00000		
3501001	00000	2			3800200	0	15023400.	1240020.0	2459350.0	0.0
3501101	000100	1			*----1---1---1---1---1---1---1---					
3501201	0	15018600.	1067100.	2459470.0	0.0	0.0	01			
3501202	0	15018600.	1173730.	2459470.0	0.0	0.0	02			
3501300	0				3850000	rabspld	branch			
3501301	.0	.0	0.0	01	3850001	1	0			
					3850101	0.0388	0.0	0.11802	0.0	-90.0
					3850102	4.0e-5	0.0	00000		-0.653
					3850200	0	15021000.	1240850.0	2459410.0	0.0
					3851101	385010000	380000000	0.0	0.0	0.0
					3851201	.212920	.260740	0.0		
					*****	*****	*****	*****	*****	*****
					*					
					* presurizer					
					*****	*****	*****	*****	*****	*****
					* surge line pcs side					
					*----1---1---1---1---1---1---1---					
					4000000	s1pcs	branch			
					4000001	2	0			
					4000101	0.00145	3.45	0.0	0.0	90.0
					4000102	4.0e-5	0.0	00000		0.54
					4000200	0	14923700.	1458370.	2461610.0	0.0
					4001101	110000000	400000000	0.00145	0.93	0.93
					100100					
					4001110	0.	0.	1.	1.	
					4002101	400010000	405000000	0.0	0.93	0.93
					4001201	-.17675e-4	-.17772e-4	0.0		
					4002201	-.17696e-5	-.17696e-5	0.0		
					*----1---1---1---1---1---1---1---					
					* surge line pressurizer vessel					
					*----1---1---1---1---1---1---1---					
					4050000	s1prv	snglvol			
					4050101	0.00145	3.45	0.0	0.0	90.0
					4050102	4.0e-5	0.0	00000		0.60
					4050200	0	14920000.	1494210.0	2461690.0	0.0
					*----1---1---1---1---1---1---1---					
					* spray line					
					*----1---1---1---1---1---1---1---					
					4060000	spray	branch			
					4060001	1	0			
					4060101	0.0003363	6.322	0.0	0.0	90.0
					4060102	3.161	4.0e-5	0.0	00000	
					4060200	0	15075000.	1244040.0	2458090.0	0.0
					4061101	406010000	420010000	2.40e-6	1.039242	1.039242
					000100					
					4061201	.08890000	.08890000	0.0		
					*----1---1---1---1---1---1---1---					
					* spray valve					
					*----1---1---1---1---1---1---1---					
					4070000	sprv1	valve			

*4070101 406010000 420010000 3.3451e-4 1.5432e1 1.5432e1 000100	4200101 0.13 0.118 0.0 0.0 90.0 0.118
*4070201 0 .000000 .000000 0.0	4200102 4.0e-5 0.0 00000
*4070300 trpvlv	4200200 0 14911300. 1541380. 2461830.0 .99907000
*4070301 690	4201101 415010000 420000000 0.0 0.0 0.0 000000
*----1----1----1----1----1----1----	4201201 -.38729 5.44472e-4 0.0
* pressurizer surge line valve	*----1----1----1----1----1----1----
*----1----1----1----1----1----1----	* porv
4100000 slvalv valve	*----1----1----1----1----1----1----
4100101 405010000 415000000 0.00145 0.93 0.93 100100	4250000 porv valve
4100110 0. 0. 1. 1.	4250101 420010000 810000000 2.4784-5 0.0 0.0 000100
4100201 0 -.17704000 -.1770400 0.0	4250102 0.8 0.03
4100300 trpvlv	4250201 0 .000000 .00000 0.0
4100301 508	4250300 trpvlv
*----1----1----1----1----1----1----	4250301 625
* pressurizer vessel	*****
*----1----1----1----1----1----1----	*
4150000 pzrve pipe	* steam generator secondary side
4150001 8	*
4150101 0.362 1	*****
4150102 0.565 5	* primary separator
4150103 0.466 7	*----1----1----1----1----1----1----
4150104 0.13 8	5000000 sepaout separatr
4150201 0.0 7	5000001 3 0
4150301 0.224 1	5000101 1.273 0.718 0.0 0.0 +90.0 +0.718
4150302 0.403 3	5000102 4.e-5 0.7874 00010
4150303 0.207 5	5000200 0 5670640. 1187483. 2592802.0 .19415000
4150304 0.1705 7	5001101 500010000 525000000 1.272800 0.0 0.0 001100 0.5
4150305 0.118 8	5002101 500000000 505000000 0.000000 0.0 0.0 001100
4150401 0.0 8	0.15
4150501 0.0 8	5003101 520000000 500000000 0.19600 0.4 0.4 001100
4150601 90.0 8	5001201 -0.4175 .75723 0.0
4150801 4.0e-5 0.0 8	5002201 0.8006 -9.39768e-2 0.0
4151001 00000 8	5003201 1.9086 4.4093 0.0
4151101 000000 7	*----1----1----1----1----1----1----
4151201 0 14917400. 1511010. 2461750.0 .0 0.0 01	* separator outlet region
4151202 0 14915500. 1568180. 2461790.0 .18395e-3 0.0 02	*----1----1----1----1----1----1----
4151203 0 14913200. 1558810. 2463620.0 .15145 0.0 03	5050000 lwrsep branch
4151203 0 14913200. 1558810. 2463620.0 .15145 0.0 03	5050001 1
4151204 0 14912100. 1582630. 2461930.0 .9996500 0.0	5050101 1.273 0.718 0.0 0.0 -90.0 -0.718
04	5050102 4.e-5 0.7874 00000
4151205 0 14911900. 1582620. 2461840.0 .9996400 0.0	5050200 0 5672780.0 1187580. 2592788.0 .01138160
05	5051101 505010000 510000000 0.0 0.0 0.0 000100
4151206 0 14911700. 1582560. 2461840.0 .9996000 0.0	5051201 0.21828 -.30041 0.0
06	*----1----1----1----1----1----1----
4151207 0 14911500. 1582300. 2461840.0 .9995300 0.0	* feed inlet volume
07	*----1----1----1----1----1----1----
4151208 0 14911400. 1575760. 2461840.0 1.0 0.0 08	5100000 feedinl branch
4151300 0	5100001 1 0
4151301 -.716473e-3 .05388 0.0 01	5100101 0.7525 0.518 0.0 0.0 -90.0 -0.518
4151302 -.62376e-3 .3445 0.0 02	5100102 4.e-5 0.10796 00000
4151303 -.27965 .12293e-2 0.0 03	5100200 0 5676840.0 1187774. 2592801.0 .408589e-5
4151304 -.27030 .17636e-3 0.0 04	5101101 510010000 515000000 0.0 0.0 0.0 000100
4151305 -.30526 .20283e-3 0.0 05	5101201 0.6328700 0.632870 0.0
4151306 -.28127 .19339e-3 0.0 06	*----1----1----1----1----1----1----
4151307 -.58439 .64379e-3 0.0 07	* steam generator downcomer
*----1----1----1----1----1----1----	*----1----1----1----1----1----1----
* pressurizer top hat and relief connection	5150000 dwncmr annulus
*----1----1----1----1----1----1----	5150001 11
4200000 toppre branch	5150101 0.23226 3
4200001 1 0	5150102 0.27871 11



5470200	1	680						
5470201	0.0	559.15	0.999					
*5470202	18000.	334.15	0.999					
*----1----1----1----1----1----1----1----1----								
* aux feed water								
*----1----1----1----1----1----1----1----1----								
5480000	auxfeed	tmdpjun						
5480101	553000000	510000000	0.10					
5480200	1	655						
5480201	-1.0	0.0	0.0	0.0				
5480202	0.0	0.0	0.0	0.0				
*5480203	0.0	2.5207	0.0	0.0				
*----1----1----1----1----1----1----1----1----								
* steam flow control valve								
*----1----1----1----1----1----1----1----1----								
5500000	cv-p4-1	valve						
5500101	530010000	535000000	0.0043266	0.0	0.0	000100		
5500201	0	19.758	22.082	0.0				
5500300	mtrvlv							
5500301	612	616	0.05	0.70	550			
*----1----1----1----1----1----1----1----1----								
* makeup feed tank								
*----1----1----1----1----1----1----1----1----								
5530000	demin	tmdpvol						
5530101	3.0	10.0	0.0	0.0	0.0	0.0		
5530102	3.33e-5	1.0	00011					
5530200	1							
5530201	0.0	366.5	0.0					
*----1----1----1----1----1----1----1----1----								
* flow path to the air cooled condenser								
*----1----1----1----1----1----1----1----1----								
5550000	coacco	sngljun						
5550101	535010000	540000000	0.0	0.0	0.0	000100		
5550201	0	13.171	36.498	0.0				
*----1----1----1----1----1----1----1----1----								
* main feed water valve								
*----1----1----1----1----1----1----1----1----								
5600000	mnfeed	tmdpjun						
5600101	545000000	510000000	0.05					
5600200	1	656						
5600201	0.0	26.533	26.533	0.0				
*****								
*								
* ecc system								
*								
*****								
* piping pcs hpis injection point								
*----1----1----1----1----1----1----1----1----								
6000000	ppchp	branch						
6000001	0	1						
6000101	0.009099	8.8776	0.0	0.0	-90.0	-3.2		
6000102	4.0e-5	0.0	00000					
6000200	0	14081300.	128835.00	2400000.0	0.000000			
*----1----1----1----1----1----1----1----1----								
* piping accumulator								
*----1----1----1----1----1----1----1----1----								
6050000	piac1	branch						
6050001	2	0						
6050101	0.014582	9.4891	0.0	0.0	0.0	0.0		
6050102	4.0e-5	0.0	00000					
6050200 0 14065600.131740.00 2600000.0 0.000000								
6051101 605010000 600000000 0.0 0.8 0.8 000100								
6052101 610010000 605000000 0.0 0.7 0.7 000100								
6051201 .98481-14.98481-14 0.0								
6052201 -.1251-13 -.1251-13 0.0								
*----1----1----1----1----1----1----1----1----								
* accumulator pipe								
*----1----1----1----1----1----1----1----1----								
6100000	piac2	snglvol						
6100101	0.018638	7.55998	0.0	0.0	0.0	0.0		
6100102	4.0-5	0.0	00000					
6100200	0	14065600.131744.	2600000.0	0.0				
*----1----1----1----1----1----1----1----1----								
* accumulator vessel								
*----1----1----1----1----1----1----1----1----								
6150000	accumlr	accum						
6150101	1.254	2.33	0.0	0.0	90.0	2.33		
6150102	4.0-5	0.0	00000					
6150200	4.37+6	304.7	0.0					
6151101	610000000	0.016817	24.6	24.6	000000			
6152200	1.97	0.0	75.13	0.0	0.04445	0 0 0 503		
*----1----1----1----1----1----1----1----1----								
* bwst lpis								
*----1----1----1----1----1----1----1----1----								
6200000	bwstlps	tmdpvol						
6200101	20.44	5.0	0.0	0.0	90.0	5.0		
6200102	4.0e-5	0.0	00000					
6200200	3							
6200201	0.0	1.0e+5	305.0					
*----1----1----1----1----1----1----1----1----								
* bwst hpis								
*----1----1----1----1----1----1----1----1----								
6250000	bwsthpis	tmdpvol						
6250101	20.44	5.0	0.0	0.0	90.0	5.0		
6250102	4.0e-5	0.0	00000					
6250200	3							
6250201	0.0	1.0e+5	305.0					
*----1----1----1----1----1----1----1----1----								
* ecc check valve								
*----1----1----1----1----1----1----1----1----								
6300000	eccvlv	valve						
6300101	600010000	185000000	0.0	0.0	0.0	000100		
6300201	0	.00000000	.00000000	0.0				
6300300	trpvlv							
6300301	502							
*----1----1----1----1----1----1----1----1----								
* low pressure injection system								
*----1----1----1----1----1----1----1----1----								
6350000	lpis	tmdpjun						
6350101	620000000	600000000	0.0					
6350200	1	635	p		205010000			
6350201	-1.0	0.0	0.0					
6350202	8.483+4	7.045	0.0	0.0				
6350203	4.297+5	6.091	0.0	0.0				
6350204	7.745+5	5.045	0.0	0.0				
6350205	9.448+5	4.313	0.0	0.0				
6350206	1.119+6	3.454	0.0	0.0				
6350207	1.186+6	3.173	0.0	0.0				
6350208	1.257+6	2.673	0.0	0.0				
6350209	1.326+6	2.159	0.0	0.0				





11004901	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	2	* mod 3
*****										
* reactor vessel heat structures										
*****										
* the reactor vessel wall is not modelled above the nozzles.										
* the vessel to filler gap is assumed to insulate the vessel										
* from the fillers. the vessel to filler gap is not modelled										
* at this elevation.										
* filler blocks inlet annulus top volume										
* station 264 to 277										
*****										
12000000	1	21	2	1	0.508					
12000100	0	1								
12000101	20	0.7264								
12000201	4	20								
12000301	0.0	20								
12000401	558.0	21								
12000501	200010000	0	1	1	0.33	1				
12000601	0	0	0	1	0.33	1				
12000701	0	0.0	0.0	0.0	1					
12000801	0.0	11.0	11.0	0.0	0.0	0.0	1.0	1	* mod 3	
*****										
* core support barrel										
* station 96.44 to 277										
*****										
12001000	6	11	2	1	0.381					
12001100	0	1								
12001101	10	0.419								
12001201	4	10								
12001301	0.0	10								
12001401	558.0	11								
12001501	0	0	0	1	0.33	1				
12001502	0	0	0	1	0.424	2				
12001503	0	0	0	1	0.958	3				
12001504	0	0	0	1	0.958	4				
12001505	0	0	0	1	0.958	5				
12001506	0	0	0	1	0.958	6				
12001601	200010000	0	1	1	0.33	1				
12001602	205010000	0	1	1	0.424	2				
12001603	210010000	0	1	1	0.958	3				
12001604	210020000	0	1	1	0.958	4				
12001605	210030000	0	1	1	0.958	5				
12001606	210040000	0	1	1	0.958	6				
12001701	0	0.0	0.0	0.0	6					
12001901	0.0	11.0	11.0	0.0	0.0	0.0	1.0	1	* mod 3	
12001902	0.0	11.0	11.0	0.0	0.0	0.0	1.0	2	* mod 3	
12001903	0.0	11.0	11.0	0.0	0.0	0.0	1.0	6	* mod 3	
*****										
* filler blocks inlet annulus lower volume										
* station 247.3 to 264.0										
*****										
12050000	1	21	2	1	0.501					
12050100	0	1								
12050101	20	0.7264								
12050201	4	20								
12050301	0.0	20								
12050401	558.0	21								
12050501	205010000	0	1	1	0.424	1				
12050601	223010000	0	1	1	0.424	1				
12050701	0	0.0	0.0	0.0	1					
*****										
12050801	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	1	* mod 3
12050901	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	1	* mod 3
*****										
* downcomer and lower plenum										
* station 67.7 to 247.3										
*****										
12100000	6	21	2	1	0.47					
12100100	0	1								
12100101	20	0.7264								
12100201	4	20								
12100301	0.0	20								
12100401	558.0	21								
12100501	210010000	0	1	1	0.958	4				
12100505	215010000	0	1	1	0.36	5				
12100506	220010000	0	1	1	0.37	6				
12100601	223020000	0	1	1	0.958	1				
12100602	223030000	0	1	1	0.958	2				
12100603	223040000	0	1	1	0.958	3				
12100604	223050000	0	1	1	0.958	4				
12100605	223060000	0	1	1	0.36	5				
12100606	223070000	0	1	1	0.37	6				
12100701	0	0.0	0.0	0.0	0.0	6				
12100801	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	4	* mod 3
12100802	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	5	* mod 3
12100803	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	6	* mod 3
12100901	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	4	* mod 3
12100902	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	5	* mod 3
12100903	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	6	* mod 3
*****										
* reactor vessel wall above station 178 - 5.50 inches thick										
* station 178 to 258 rv not modelled above bottom of nozzles										
*****										
12110000	3	11	2	1	0.7328					
12110100	0	1								
12110101	10	0.8725								
12110201	5	10								
12110301	0.0	10								
12110401	558.0	11								
12110501	223010000	0	1	1	0.424	1				
12110502	223020000	0	1	1	0.958	2				
12110503	223030000	0	1	1	0.6500	3				
12110601	-939	0	3949	1	0.424	1				
12110602	-939	0	3949	1	0.958	2				
12110603	-939	0	3949	1	0.6500	3				
12110701	0	0.0	0.0	0.0	0.0	3				
12110801	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	1	* mod 3
12110802	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	2	* mod 3
12110803	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	3	* mod 3
*****										
* reactor vessel wall bellow station 178 - 3.62 inches thick										
* station 67.7 to 178										
*****										
12120000	5	7	2	1	0.7328					
12120100	0	1								
12120101	6	0.8247								
12120201	5	6								
12120301	0.0	6								
12120401	558.0	7								
12120501	223030000	0	1	1	0.308	1				
12120502	223040000	10000	1	1	0.958	3				

12120503	223060000	0	1	1	0.3600	4	
12120504	223070000	0	1	1	0.37	5	
12120601	-939	0	3949	1	0.308	1	
12120602	-939	0	3949	1	0.958	3	
12120603	-939	0	3949	1	0.36	4	
12120604	-939	0	3949	1	0.37	5	
12120701	0	0.0	0.0	0.0	5		
12120801	0.0	11.0	11.0	0.0	0.0	0.0	1.0 1 * mod 3
12120802	0.0	11.0	11.0	0.0	0.0	0.0	1.0 3 * mod 3
12120803	0.0	11.0	11.0	0.0	0.0	0.0	1.0 4 * mod 3
12120804	0.0	11.0	11.0	0.0	0.0	0.0	1.0 5 * mod 3
*****							
* reactor vessel bottom station 67.7							
*****							
12200000	1	11	1	1	0.0		
12200100	0	1					
12200101	10	0.092					
12200201	5	10					
12200301	0.0	10					
12200401	558.0	11					
12200501	220010000	0	1	0	1.68	1	
12200601	-939	0	3949	0	1.68	1	
12200701	0	0.0	0.0	0.0	1		
12200801	0.0	11.0	11.0	0.0	0.0	0.0	1.0 1 * mod 3
12200901	0.0	11.0	11.0	0.0	0.0	0.0	1.0 1 * mod 3
*****							
* flow skirt - core filler assembly station 96.44 to 261.13							
*****							
12250000	7	11	2	1	0.3		
12250100	0	1					
12250101	10	0.38					
12250201	4	10					
12250301	0.0	10					
12250401	558.0	11					
12250501	225010000	0	1	1	0.52	1	
12250502	230010000	0	1	1	0.559	2	
12250503	230020000	0	1	1	0.559	3	
12250504	230030000	0	1	1	0.657	4	
12250505	240010000	0	1	1	1.118	5	
12250506	245010000	0	1	1	0.42	6	
12250507	246010000	0	1	1	0.35	7	
12250601	0	0	0	1	0.52	1	
12250602	0	0	0	1	0.559	2	
12250603	0	0	0	1	0.559	3	
12250604	0	0	0	1	0.657	4	
12250605	0	0	0	1	1.118	5	
12250606	0	0	0	1	0.42	6	
12250607	0	0	0	1	0.35	7	
12250701	0	0.0	0.0	0.0	7		
12250801	0.0	11.0	11.0	0.0	0.0	0.0	1.0 1 * mod 3
12250802	0.0	11.0	11.0	0.0	0.0	0.0	1.0 3 * mod 3
12250803	0.0	11.0	11.0	0.0	0.0	0.0	1.0 4 * mod 3
12250804	0.0	11.0	11.0	0.0	0.0	0.0	1.0 5 * mod 3
12250805	0.0	11.0	11.0	0.0	0.0	0.0	1.0 6 * mod 3
12250806	0.0	11.0	11.0	0.0	0.0	0.0	1.0 7 * mod 3
*****							
* lower core support structure station 96.44 to 116.91							
* includes core support barrel lip , lower core support							
* structure , and fuel module lower end boxes							
12260000	1	7	2	1	0.282		
12260100	0	1					
12260101	6	0.3					
12260201	4	6					
12260301	0.0	6					
12260401	558.0	7					
12260501	225010000	0	1	1	0.52	1	
12260601	0	0	0	1	0.52	1	
12260701	0	0.0	0.0	0.0	1		
12260801	0.0	11.0	11.0	0.0	0.0	0.0	1.0 1 * mod 3
12260901	0.0	11.0	11.0	0.0	0.0	0.0	1.0 1 * mod 3
12300000	3	10	2	1	0.0		
12300100	0	1					
12300101	5	4.647e-3					
12300102	1	4.742e-3					
12300103	3	5.359e-3					
12300201	1	5					
12300202	2	6					
12300203	3	9					
12300301	1.0	5					
12300302	0.0	9					
12300401	558.0	10					
12300501	0	0	0	1	725.1	3	
12300601	230010000	0	1	1	725.1	1	
12300602	230020000	0	1	1	725.1	2	
12300603	230030000	0	1	1	725.1	3	
12300701	1000	0.41209	0.0	0.0	1		
12300702	1000	0.44565	0.0	0.0	2		
12300703	1000	0.14226	0.0	0.0	3		
12300901	0.0124	11.0	11.0	0.0	0.0	0.0	1.0 3 * mod 3
*****							
* upper core support structure station 190.5 to 234.5							
*****							
12400000	1	7	2	1	0.282		
12400100	0	1					
12400101	6	0.31					
12400201	4	6					
12400301	0.0	6					
12400401	558.0	7					
12400501	240010000	0	1	1	1.118	1	
12400601	0	0	0	1	1.118	1	
12400701	0	0.0	0.0	0.0	1		
12400801	0.0	11.0	11.0	0.0	0.0	0.0	1.0 1 * mod 3
*****							
* fuel modules station 187.6 to 258.4							
*****							
12460000	1	5	1	1	0.0		
12460100	0	1					
12460101	4	0.01					
12460201	4	4					
12460301	0.0	4					
12460401	558.0	5					
12460501	245010000	0	1	1	1.8	1	
12460601	246010000	0	1	1	1.8	1	
12460701	0	0.0	0.0	1.8	1		
12460801	0.0	11.0	11.0	0.0	0.0	0.0	1.0 1 * mod 3
12460901	0.0	11.0	11.0	0.0	0.0	0.0	1.0 1 * mod 3

*****							
* core support barrel - upper plenum lower volume							
* station 264 to 297.6							
* reactor vessel not modelled above bottom of nozzles							
* the vessel to filler gap is assumed to insulate the vessel							
* from the fillers. the vessel to filler gap is not modelled							
* at this elevation.							
*****							
12500000	1	11	2	1	0.381	12550601	-939
12500100	0	1				12550701	0
12500101	10	0.419				12550801	0.0
12500201	5	10				12550	11.0
12500301	0.0	10				12550	11.0
12500401	558.0	11				12550	0.0
12500501	250010000	0	1	1	0.854	12550	0.0
12500601	0	0	0	1	0.854	12550	0.0
12500701	0	0.0	0.0	0.0	1	12550	0.0
12500801	0.0	11.0	11.0	0.0	0.0	12550	0.0
*****							
* internals upper plenum							
*****							
12510000	2	5	1	1	0.0	13151000	1
12510100	0	1				13151100	0
12510101	4	0.005				13151101	10
12510201	4	4				13151201	4
12510301	0.0	4				13151301	0.0
12510401	558.0	5				13151401	540.0
12510501	250010000	0	1	1	1.0	13151501	315090000
12510502	250010000	0	1	1	1.0	13151601	-939
12510601	0	0	0	1	1.0	13151701	0
12510701	0	0.0	0.0	0.0	2	13151801	0.0
12510801	0.0	11.0	11.0	0.0	0.0	13152000	1
*****							
* core support barrel - upper plenum top volume							
* station 297.6 to 325							
* reactor vessel not modelled above bottom of nozzles							
* the vessel to filler gap is assumed to insulate the vessel							
* from the fillers. the vessel to filler gap is not modelled							
* at this elevation.							
*****							
12501000	1	21	2	1	0.381	13152100	0
12501100	0	1				13152101	10
12501101	20	0.728				13152201	4
12501201	5	20				13152301	0.0
12501301	0.0	20				13152401	540.0
12501401	558.0	21				13152501	315110000
12501501	250010000	0	1	1	0.712	13152601	-939
12501601	0	0	0	1	0.712	13152701	0
12501701	0	0.0	0.0	0.0	1	13152801	0.0
12501801	0.0	11.0	11.0	0.0	0.0	13153000	6
*****							
* upper head top plate station 325							
*****							
12550000	1	21	1	1	0.0	13154000	1
12550100	0	1				13154100	0
12550101	20	0.474				13154101	10
12550201	5	20				13154201	4
12550301	0.0	20				13154301	0.0
12550401	558.0	21				13154401	540.0
12550501	250010000	0	1	1	0.712	13154501	315120000

13154601	-939	0	3979	1	0.0525	1		13501401	540.0	11				
13154701	0	0	0	0	1			13501501	350010000	0	1	1	0.488	1
13154801	0.0	11.0	11.0	0.0	0.0	0.0	1.0	1	* mod 3					
*****														
13155000	1	11	2	1	0.1420			13501601	-939	0	3949	1	0.488	1
13155100	0	1						13501701	0	0	0	0	1	
13155101	10	0.1780						13501801	0.0	11.0	11.0	0.0	0.0	1.0
13155201	4	10						1	* mod 3					
13155301	0.0	10												
13155401	540.0	11												
13155501	315100000	0	1	1	0.0489057	1								
13155601	-939	0	3979	1	0.0489057	1								
13155701	0	0	0	0	1									
13155801	0.0	11.0	11.0	0.0	0.0	0.0	1.0	1	* mod 3					
*****														
* nozzle piping														
*****														
13000000	3	11	2	1	0.1420									
13000100	0	1												
13000101	10	0.1780												
13000201	4	10												
13000301	0.0	10												
13000401	540.0	11												
13000501	300010000	0	1	1	0.876	1								
13000502	305010000	0	1	1	0.698	2								
13000503	310010000	0	1	1	1.424	3								
13000601	-939	0	3979	1	0.876	1								
13000602	-939	0	3979	1	0.698	2								
13000603	-939	0	3979	1	1.424	3								
13000701	0	0	0	0	3									
13000801	0.0	11.0	11.0	0.0	0.0	0.0	1.0	1	* mod 3					
13000802	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	2	* mod 3				
13000803	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	3	* mod 3				
*****														
* broken loop cold leg														
*****														
* nozzle piping														
*****														
13350000	3	11	2	1	0.1420									
13350100	0	1												
13350101	10	0.1780												
13350201	4	10												
13350301	0.0	10												
13350401	540.0	11												
13350501	335010000	0	1	1	0.7495	1								
13350502	340010000	0	1	1	0.698	2								
13350503	345010000	0	1	1	0.974	3								
13350601	-939	0	3949	1	0.7495	1								
13350602	-939	0	3949	1	0.698	2								
13350603	-939	0	3949	1	0.974	3								
13350701	0	0	0	0	3									
13350801	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	1	* mod 3				
13350802	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	2	* mod 3				
13350803	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	3	* mod 3				
*****														
* vessel bottom														
*****														
14151000	1	11	1	1	1	1	0.0							
14151100	0	1												
14151101	10	0.0762												
14151201	5	10												
14151301	0.0	10												
14151401	617.0	11												
14151501	415010000	0	1	1	0.362	1								
14151601	-939	0	3969	1	0.362	1								
14151701	0	0	0	0	1									
14151801	0.0	11.0	11.0	0.0	0.0	0.0	0.0	0.0	1.0	1	* mod 3			
*****														
* vessel sides - large diameter section														
*****														
14152000	7	11	2	1	0.42291									
14152100	0	1												
14152101	10	0.49911												
14152201	5	10												





20100352	1077.6	2.312e6		20100754	533.15	1938.87
20100353	1185.9	5.712e6		20100755	588.71	1906.01
20100354	1248.4	2.311e6		20100756	644.26	1873.15
20100355	2199.8	2.312e6		20100757	699.82	1840.29
*----1----	-----1-----1-----1-----1-----1---			20100758	755.37	1807.43
* s-steel - volumetric heat capacity				20100759	810.93	1774.56
*----1----	-----1-----1-----1-----1-----1---			20100760	866.48	1741.70
20100451	273.15	3.83e6		20100761	922.04	1708.84
20100452	366.5	3.83e6		20100762	977.59	1675.96
20100453	1366.5	5.376e6		20100763	1033.15	1643.11
*----1----	-----1-----1-----1-----1-----1---			20100764	1088.71	1610.25
* inconel-600 - volumetric heat capacity				20100765	1144.26	1577.39
*----1----	-----1-----1-----1-----1-----1---			20100766	1199.82	1544.53
20100651	366.5	3.908+6		20100767	1255.37	1511.67
20100652	477.6	4.084+6		20100768	1310.93	1478.80
20100653	588.7	4.260+6		20100769	1366.48	1445.94
20100654	700.0	4.436+6		20100770	1422.04	1413.08
20100656	810.9	4.665+6		20100771	1477.59	1380.22
20100657	922.0	4.929+6		20100772	1533.15	1347.35
20100658	1033.2	5.105+6		20100773	1588.71	1314.49
20100659	1477.6	5.727+6		20100774	1644.26	1281.63
*----1----	-----1-----1-----1-----1-----1---			20100775	1699.82	1248.77
* magnesium oxide - thermal conductivity				20100776	1755.37	1215.90
*----1----	-----1-----1-----1-----1-----1---			20100777	1810.93	1183.04
20100701	373.15	0.2451		20100778	1866.48	1150.18
20100702	422.04	0.2405		20100779	1922.04	1117.32
20100703	477.59	0.2352		20100780	5000.00	1117.32
20100704	533.15	0.2300		*----1----	-----1-----1-----1-----1-----1---	
20100705	588.71	0.2249		* nichrome - thermal conductivity		
20100706	644.26	0.2196		*----1----	-----1-----1-----1-----1-----1---	
20100707	699.82	0.2143		20100801	373.15	1.1163
20100708	755.37	0.2091		20100802	1922.04	1.1163
20100709	810.93	0.2039		20100803	5000.00	1.1163
20100710	866.48	0.1987		*----1----	-----1-----1-----1-----1-----1---	
20100711	922.04	0.1934		* nichrome - volumetric heat capacity		
20100712	977.59	0.1882		*----1----	-----1-----1-----1-----1-----1---	
20100713	1033.15	0.1830		20100851	373.15	2180.80
20100714	1088.71	0.1777		20100852	1922.04	2180.80
20100715	1144.26	0.1725		20100853	5000.00	2180.80
20100716	1199.82	0.1673		*----1----	-----1-----1-----1-----1-----1---	
20100717	1255.37	0.1621		* pressurizer cycling heaters		
20100718	1310.93	0.1568		*----1----	-----1-----1-----1-----1-----1---	
20100719	1366.48	0.1516		20241700	power	608
20100720	1422.04	0.1464		20241701	0.0	0.0
20100721	1477.59	0.1412		20241702	60.	4.e3
20100722	1533.15	0.1359		*----1----	-----1-----1-----1-----1-----1---	
20100723	1588.71	0.1307		* pressurizer backup heaters		
20100724	1644.26	0.1255		*----1----	-----1-----1-----1-----1-----1---	
20100725	1699.82	0.1203		20241800	power	629
20100726	1755.37	0.1150		20241801	0.0	0.0
20100727	1810.93	0.1098		20241802	60.	4.e3
20100728	1866.48	0.1046		*----1----	-----1-----1-----1-----1-----1---	
20100729	1922.04	0.0993		* scram reactivity data		
20100730	5000.00	0.0993		*----1----	-----1-----1-----1-----1-----1---	
*----1----	-----1-----1-----1-----1-----1---			20260900	"react-t "	609
* magnesium oxide - volumetric heat capacity				20260901	0.0	0.0
*----1----	-----1-----1-----1-----1-----1---			20260902	0.5	-0.5
20100751	373.15	2033.52		20260903	0.59	-3.13
20100752	422.04	2004.59		20260904	0.65	-3.95
20100753	477.59	1917.74		20260905	0.75	-6.27

20260906	0.83	-8.72		20290013	65.0	1.7115e6
20260907	0.90	-12.00		20290014	100.0	1.5425994e6
20260908	0.97	-17.12		20290015	250.0	1.232769e6
20260909	1.125	-20.67		20290016	650.0	0.91932e6
20260910	1.213	-22.10		20290017	1000.0	0.80196e6
20260911	1.3	-22.78		20290018	1500.0	0.6846e6
20260912	1.4	-23.17		20290019	3000.0	0.5379e6
20260913	1.6	-23.32		20290020	5000.0	0.44988e6
20260914	60.0	-23.32				*****
*----1----1----1----1----1----1----1----1----				*		
* reactor power table				*		
*----1----1----1----1----1----1----1----1----				*		
20290000	power					reactor kinetics data
20290001	0.0	48.9e6		*		
*----1----1----1----1----1----1----1----1----				*		
* environmental heat loss boundary temperature				*		
*----1----1----1----1----1----1----1----1----						*****
20293900	temp					* delayed neutron constants
20293901	0.0	311.0				*****
*----1----1----1----1----1----1----1----1----						
* reactor vessel environmental loss heat xfer coefficient				30000101	0.0349	0.01275
*----1----1----1----1----1----1----1----1----				30000102	0.2035	0.03177
20294900	htc-t			30000103	0.1848	0.1181
20294901	0.0	18.83		30000104	0.4046	0.3160
*----1----1----1----1----1----1----1----1----				30000105	0.1401	1.402
* steam generator environmental loss heat xfer coefficient				30000106	0.0321	3.914
*----1----1----1----1----1----1----1----1----						*****
20295900	htc-t					* power history
20295901	0.0	4.739				*****
*----1----1----1----1----1----1----1----1----				30000401	4.96e+7	70. hr
* pressurizer generator environmental loss heat xfer coefficient						*****
*----1----1----1----1----1----1----1----1----						* reactivity curve numbers
20296900	htc-t					*****
20296901	0.0	4.2266		30000011	609	
*----1----1----1----1----1----1----1----1----						*****
* blhl environmental loss heat xfer coefficient						* moderator density reactivity table
*----1----1----1----1----1----1----1----1----						*****
20297900	htc-t	509		*30000501	0.818	-4.428
20297901	-1.0	0.0		*30000502	0.905	-2.249
20297902	0.0	18.83		*30000503	0.955	-1.032
*****				*30000504	1.000	0.000
* core collapsed liquid level				*30000505	1.044	0.926
*****				*30000506	1.095	1.853
20255000	normarea	0 1.0 1.0		*30000507	1.139	2.589
20255001	0.0	9.25e-4		*30000508	1.213	3.689
20255002	9.25e-4	9.25e-4		*30000509	1.270	4.489
20255003	1.0	1.0		*30000510	1.316	5.212
20290000	power	609				*****
20290001	0.0	48.9e-6				* doppler reactivity table
20290002	0.15	43.032e6				*****
20290003	0.3	37.164e6		*30000601	293.16	1.375
20290004	0.6	28.362e6		*30000602	338.72	1.125
20290005	0.85	8.6064e6		*30000603	422.05	0.682
20290006	1.0	5.99538e6		*30000604	477.60	0.419
20290007	1.3	4.89e6		*30000605	505.38	0.274
20290008	2.0	4.274e6		*30000606	570.72	0.000
20290009	4.0	3.7060332e6		*30000607	588.72	-0.075
20290010	7.0	3.1296e6		*30000608	695.83	-0.526
20290011	10.0	2.93458e6		*30000609	922.05	-1.386
20290012	25.0	2.28548e6		*30000610	1310.94	-2.543
				*30000611	1810.94	-3.865

*30000612 2088.72 -4.502	20500104 0.7102 voidf 515010000
*30000613 2499.83 -5.392	20500105 0.7102 voidf 515020000
*30000614 3027.60 -6.417	20500106 0.7102 voidf 515030000
*****	
* moderator density reactivity table	*----1----1----1----1----1----1----
*****	
30000501 0.818 0.0	20500200 pzrlvl sum 1.0 0.0 1
30000502 0.905 0.0	20500201 0.0 0.224 voidf 415010000
30000503 0.955 0.0	20500202 0.403 voidf 415020000
30000504 1.000 0.0	20500203 0.403 voidf 415030000
30000505 1.044 0.0	20500204 0.207 voidf 415040000
30000506 1.095 0.0	20500205 0.207 voidf 415050000
30000507 1.139 0.0	20500206 0.1705 voidf 415060000
30000508 1.213 0.0	20500207 0.1705 voidf 415070000
30000509 1.270 0.0	20500208 0.118 voidf 415080000
30000510 1.316 0.0	20500209 0.118 voidf 420010000
*****	
* doppler reactivity table	*----1----1----1----1----1----1----
*****	
30000601 293.16 0.0	20500300 rvlvl sum 1.0 0.0 1
30000602 338.72 0.0	20500301 0.0 0.712 voidf 250010000
30000603 422.05 0.0	20500302 0.854 voidf 250010000
30000604 477.60 0.0	20500303 0.843 voidf 245010000
30000605 505.38 0.0	20500304 1.118 voidf 240010000
30000606 570.72 0.0	20500305 0.657 voidf 230030000
30000607 588.72 0.0	20500306 0.559 voidf 230020000
30000608 695.83 0.0	20500307 0.559 voidf 230010000
30000609 922.05 0.0	20500308 0.520 voidf 225010000
30000610 1310.94 0.0	20500309 0.360 voidf 215010000
30000611 1810.94 0.0	20500310 0.370 voidf 220010000
30000612 2088.72 0.0	*----1----1----1----1----1----1----
30000613 2499.83 0.0	* hot leg intact loop
30000614 3027.60 0.0	*----1----1----1----1----1----1----
* ----- no reactivity feedback for steady state run	20504100 pcsvol1 sum 1.0 0.0 1
* ----- shoud be replaced by original one for transient	20504101 0.0 .09746482 rho 100010000
*****	
* volume weighting factors	20504102 0.1035956 rho 105010000
*****	
* moderator temperature feedback	20504103 3.0300e-2 rho 110010000
*****	
30000701 230010000 0 0.31493 0.0	20504104 9.0000e-2 rho 115010000
30000702 230020000 0 0.31493 0.0	20504105 5.7000e-2 rho 115020000
30000703 230030000 0 0.37014 0.0	*----1----1----1----1----1----1----
*****	
* doppler feedback	* steam generator
*****	
30000801 2300001 0 0.43153 0.0	*----1----1----1----1----1----1----
30000802 2300002 0 0.51686 0.0	20504200 pcsvol2 sum 1.0 0.0 1
30000803 2300003 0 0.05161 0.0	20504201 0.0 0.3350000 rho 115030000
*****	
*	20504202 0.0402793 rho 115040000
* control variables	20504203 0.0402793 rho 115050000
*	20504204 0.0402793 rho 115060000
*----1----1----1----1----1----1----	20504205 0.0402793 rho 115070000
* steam generator downcomer collapsed liquid level	20504206 1.61117-1 rho 115080000
*----1----1----1----1----1----1----	20504207 6.7950e-2 rho 115090000
*	20504208 6.7950e-2 rho 115100000
* control variables	20504209 1.61117-1 rho 115110000
*	20504210 0.0402793 rho 115120000
*----1----1----1----1----1----1----	20504211 0.0402793 rho 115130000
* steam generator downcomer collapsed liquid level	20504212 0.0402793 rho 115140000
*----1----1----1----1----1----1----	20504213 0.0402793 rho 115150000
20500100 sglvl sum 1.0 0.0 1	20504214 3.3500e-1 rho 115160000
20500101 0.0 0.718 voidf 500010000	*----1----1----1----1----1----1----
20500102 0.718 voidf 505010000	* sg-pump piping
20500103 0.518 voidf 510010000	*----1----1----1----1----1----1----

20504300	pcsvol3	sum	1.0	0.0	1	
20504301	0.0	4.37000-2 rho	115170000			
20504302		4.62000-2 rho	115180000			
20504303		3.54406-2 rho	115190000			
20504304		4.81840-2 rho	120010000			
20504305		6.13000-2 rho	125010000			
20504306		1.89000-2 rho	130010000			
20504307		6.13000-2 rho	155010000			
20504308		1.89000-2 rho	160010000			
*----1----	-----1----	-----1----	-----1----			
* cold leg intact loop						
*----1----	-----1----	-----1----	-----1----			
20500400	pcsvol4	sum	1.0	0.0	1	
20500401	0.0	9.90000-2 rho	135010000			
20500402		1.83732-2 rho	140010000			
20500403		6.33000-2 rho	145010000			
20500404		3.14844-2 rho	150010000			
20500405		9.90000-2 rho	165010000			
20500406		1.88124-2 rho	170010000			
20500407		3.54406-2 rho	175010000			
20500408		3.88642-2 rho	175020000			
20500409		4.44434-2 rho	180010000			
20500410		9.26274-2 rho	185010000			
*----1----	-----1----	-----1----	-----1----			
* reactor						
*----1----	-----1----	-----1----	-----1----			
20500500	pcsvol5	sum	1.0	0.0	1	
20500501	0.0	2.66400-1 rho	215010000			
20500502		2.92300-1 rho	220010000			
20500503		1.30000-1 rho	225010000			
20500504		9.53095-2 rho	230010000			
20500505		9.53095-2 rho	230020000			
20500506		0.1120185 rho	230030000			
20500507		8.38500-3 rho	235010000			
20500508		8.38500-3 rho	235020000			
20500509		9.35500-3 rho	235030000			
20500510		3.32046-1 rho	240010000			
20500511		9.61020-2 rho	245010000			
20500512		1.28100-1 rho	246010000			
20500513		2.45952-1 rho	250010000			
20500514		1.73728-1 rho	250010000			
*----1----	-----1----	-----1----	-----1----			
* hot leg broken loop						
*----1----	-----1----	-----1----	-----1----			
20500600	pcsvol6	sum	1.0	0.0	1	
20500601	0.0	5.55384-2 rho	300010000			
20500602		4.42532-2 rho	305010000			
20500603		6.68000-2 rho	310010000			
20500604		3.38914-3 rho	315010000			
20500605		4.40154-3 rho	315020000			
20500606		3.90960-2 rho	315030000			
20500607		1.82736-1 rho	315040000			
20500608		9.17460-2 rho	315050000			
20500609		9.17460-2 rho	315060000			
20500610		1.82736-1 rho	315070000			
20500611		3.90960-2 rho	315080000			
20500612		1.62000-2 rho	315090000			
20500613		6.48000-2 rho	315100000			
20500614		.01539912 rho	315110000			
20500615		3.50175-2 rho	315120000			
20500616			8.54764-2 rho	370010000		
20500617			8.58000-2 rho	375010000		
*----1----	-----1----	-----1----	-----1----			
* cold leg broken loop						
*----1----	-----1----	-----1----	-----1----			
20500700	pcsvol7	sum	1.0	0.0	1	
20500701	0.0	4.75183-2 rho	335010000			
20500702		4.42532-2 rho	340010000			
20500703		6.17516-2 rho	345010000			
20500704		5.41000-3 rho	350010000			
20500705		0.07770 rho	350020000			
20500706		8.55000-2 rho	380010000			
20500707		1.18030-1 rho	385010000			
*----1----	-----1----	-----1----	-----1----			
* pressurizer						
*----1----	-----1----	-----1----	-----1----			
20500800	pcsvol8	sum	1.0	0.0	1	
20500801	0.0	5.00250-3 rho	400010000			
20500802		5.00250-3 rho	405010000			
20500803		8.10880-2 rho	415010000			
20500804		2.27695-1 rho	415020000			
20500805		2.27695-1 rho	415030000			
20500806		1.16955-1 rho	415040000			
20500807		1.16955-1 rho	415050000			
20500808		7.94530-2 rho	415060000			
20500809		7.94530-2 rho	415070000			
20500810		1.53400-2 rho	415080000			
*----1----	-----1----	-----1----	-----1----			
* reactor vessel downcomer mass						
*----1----	-----1----	-----1----	-----1----			
20500900	dwncrms	sum	1.0	0.0	1	
20500901	0.0	8.55000-2 rho	200010000			
20500902		1.10000-1 rho	205010000			
20500903		1.36036-1 rho	210010000			
20500904		1.36036-1 rho	210020000			
20500905		1.36036-1 rho	210030000			
20500906		1.36036-1 rho	210040000			
20500907		1.23426-2 rho	223010000			
20500908		2.78874-2 rho	223020000			
20500909		2.78874-2 rho	223030000			
20500910		2.78874-2 rho	223040000			
20500911		2.78874-2 rho	223050000			
20500912		1.04796-2 rho	223060000			
20500913		1.04796-2 rho	223070000			
*----1----	-----1----	-----1----	-----1----			
* pcs mass						
*----1----	-----1----	-----1----	-----1----			
20501000	pcsmass	sum	1.0	0.0	1	
20501001	0.0	1.0	cntrlvar 41			
20501002		1.0	cntrlvar 42			
20501003		1.0	cntrlvar 43			
20501004		1.0	cntrlvar 4			
20501005		1.0	cntrlvar 5			
20501006		1.0	cntrlvar 6			
20501007		1.0	cntrlvar 7			
20501008		1.0	cntrlvar 8			
20501009		1.0	cntrlvar 9			
*----1----	-----1----	-----1----	-----1----			
* break energy computer						
*----1----	-----1----	-----1----	-----1----			

20542500	pvfstm	div	1.0	0.0	1		*----1----1----1----1----1----1----1----
20542501	rhof	420010000 p		420010000		20511300	rvheat sum 1.0 0.0 1
*						20511301	0.0 2.3244 htrnr 211000101
20542600	hfstm	sum	1.0	0.0	1	20511302	5.25183 htrnr 211000201
20542601	0.0	1.0	uf	420010000		20511303	3.56335 htrnr 211000301
20542602		1.0	cntrlvar	425		20511304	1.59598 htrnr 212000101
*						20511305	4.96411 htrnr 212000201
20542700	pvgstm	div	1.0	0.0	1	20511306	4.96411 htrnr 212000301
20542701	rhog	420010000 p		420010000		20511307	1.86543 htrnr 212000401
*						20511308	1.91724 htrnr 212000501
20542800	hgstm	sum	1.0	0.0	1	20511309	1.68000 htrnr 220000101
20542801	0.0	1.0	ug	420010000		20511310	0.71200 htrnr 255000101
20542802		1.0	cntrlvar	427		*	*----1----1----1----1----1----1----
*						*	heat loss from pqr
20542900	xhgstm	mult	1.0	0.0	1	*	*----1----1----1----1----1----1----
20542901	quals	420010000 cntrlvar	428			20511400	pzrheat sum 1.0 0.0 1
*						20511401	0.0 0.362 htrnr 415100101
20543000	xhfstm	mult	1.0	0.0	1	20511402	0.702464 htrnr 415200101
20543001	quals	420010000 cntrlvar	426			20511403	1.26381 htrnr 415200201
*						20511404	1.26381 htrnr 415200301
20543100	yhfstm	sum	1.0	0.0	1	20511405	0.649152 htrnr 415200401
20543101	0.0	1.0	cntrlvar	426		20511406	0.649152 htrnr 415200501
20543102		-1.0	cntrlvar	430		20511407	0.534688 htrnr 415200601
*						20511408	0.534688 htrnr 415200701
20543200	hsteam	sum	1.0	0.0	1	20511409	0.273063 htrnr 416200101
20543201	0.0	1.0	cntrlvar	429		20511410	0.130000 htrnr 420100101
20543202		1.0	cntrlvar	431		20511411	0.273063 htrnr 420200101
*						*	*----1----1----1----1----1----1----
20543300	brkpwr	mult	1.0	0.0	1	*	heat loss from s/g
20543301	mflowj	425000000 cntrlvar	432			*	*----1----1----1----1----1----1----
*						20511500	sgheat sum 1.0 0.0 1
20543400	brkflow	integral	1.0	0.0	1	20511501	0.0 3.5343 htrnr 530000101
20543401	mflowj	425000000				20511502	3.5343 htrnr 530000201
*----1----1----1----1----1----1----						20511503	3.33022 htrnr 530000301
* 011 - 031 heat transfer rate calculator						20511504	3.33022 htrnr 530000401
*----1----1----1----1----1----1----						20511505	2.40258 htrnr 530000501
* heat added to pcs from core						20511506	3.29404 htrnr 530000601
*----1----1----1----1----1----1----						20511507	3.29404 htrnr 530000701
20511100	corhtr	sum	1.0	0.0	1	20511508	3.29404 htrnr 530000801
20511101	0.0	24.374	htnr	230000101		*	*----1----1----1----1----1----1----
20511102		24.374	htnr	230000201		*	total heat loss from major components
20511103		24.374	htnr	230000301		*	*----1----1----1----1----1----1----
*----1----1----1----1----1----1----						20511600	toheat sum 1.0 0.0 1
* heat removed from pcs at to s/g tubes						20511601	0.0 1.0 cntrlvar 113
*----1----1----1----1----1----1----						20511602	1.0 cntrlvar 114
20511200	sghttr	sum	1.0	0.0	1	20511603	1.0 cntrlvar 115
20511201	0.0	20.117	htnr	006000100		*	*----1----1----1----1----1----1----
20511202		20.117	htnr	006000200		*	heat loss from broken loop hot leg
20511203		20.117	htnr	006000300		*	*----1----1----1----1----1----1----
20511204		20.117	htnr	006000400		20511700	blhlheat sum 1.0 0.0 1
20511205		80.468	htnr	006000500		20511701	0.0 0.97972 htrnr 300000101
20511206		33.937	htnr	006000600		20511702	0.78065 htrnr 300000201
20511207		33.937	htnr	006000700		20511703	1.59260 htrnr 300000301
20511208		80.468	htnr	006000800		*	*----1----1----1----1----1----1----
20511209		20.117	htnr	006000900		*	heat loss from broken loop cold leg
20511210		20.117	htnr	006001000		*	*----1----1----1----1----1----1----
20511211		20.117	htnr	006001100		20511800	bldheat sum 1.0 0.0 1
20511212		20.117	htnr	006001200		20511801	0.0 0.83825 htrnr 335000101
*----1----1----1----1----1----1----						20511802	0.78065 htrnr 335000201
* heat loss from reactor vessel						20511803	1.0893 htrnr 335000301

\*----1----1----1----1----1----1----1----1----  
 \* heat loss from rabs piping  
 \*----1----1----1----1----1----1----1----  
 20511900 rabheat sum 1.0 0.0 1  
 20511901 0.0 1.7153 htrnr 370000101  
 20511902 0.94828 htrnr 370000201  
 20511903 0.94497 htrnr 370000301  
 20511904 2.6090 htrnr 370000401  
 \*----1----1----1----1----1----1----1----  
 \* heat loss from intact loop hot leg  
 \*----1----1----1----1----1----1----1----  
 20512000 ildheat sum 1.0 0.0 1  
 20512001 0.0 1.7193 htrnr 100100101  
 20512002 1.8275 htrnr 100100201  
 20512003 0.69677 htrnr 100100301  
 20512004 1.6088 htrnr 100100401  
 20512005 0.90304 htrnr 100200101  
 20512006 1.8855 htrnr 100400101  
 \*----1----1----1----1----1----1----1----  
 \* heat loss from intact loop cold leg  
 \*----1----1----1----1----1----1----1----  
 20512100 ildheat sum 1.0 0.0 1  
 20512101 0.0 0.77058 htrnr 100100501  
 20512102 0.62519 htrnr 100100601  
 20512103 0.84999 htrnr 100100701  
 20512104 0.55540 htrnr 100100801  
 20512105 0.62519 htrnr 100100901  
 20512106 0.68558 htrnr 100101001  
 20512107 0.78400 htrnr 100101101  
 20512108 1.6340 htrnr 100101201  
 20512109 0.69769 htrnr 100200201  
 20512110 0.85765 htrnr 100300101  
 20512111 0.39195 htrnr 100300201  
 20512112 0.43054 htrnr 100300301  
 20512113 1.2079 htrnr 100300401  
 20512114 0.86023 htrnr 100300501  
 20512115 0.39195 htrnr 100300601  
 20512116 0.44083 htrnr 100300701  
 20512117 1.8855 htrnr 100400201  
 \*----1----1----1----1----1----1----1----  
 \* total heat loss to environment  
 \*----1----1----1----1----1----1----1----  
 20512200 sumhtls sum 1.0 0.0 1  
 20512201 0.0 1.0 cntrlvar 116  
 20512202 1.0 cntrlvar 117  
 20512203 1.0 cntrlvar 118  
 20512204 1.0 cntrlvar 119  
 20512205 1.0 cntrlvar 120  
 20512206 1.0 cntrlvar 121  
 \*----1----1----1----1----1----1----1----  
 \* metal heating in pzs  
 \*----1----1----1----1----1----1----1----  
 20512300 pzrmtht sum 1.0 0.0 1  
 20512301 0.0 0.3620 htrnr 415100100  
 20512302 0.59522 htrnr 415200100  
 20512303 1.07086 htrnr 415200200  
 20512304 1.07086 htrnr 415200300  
 20512305 0.550045 htrnr 415200400  
 20512306 0.550045 htrnr 415200500  
 20512307 0.453056 htrnr 415200600

20512308	0.453056	htrnr	415200700
20512309	0.150656	htrnr	416200100
20512310	0.13000	htrnr	420100100
20512311	0.150656	htrnr	420200100
*----1----1----1----1----1----1----1----			
* metal heating in reactor vessel (1st part)			
*----1----1----1----1----1----1----1----			
20525100 rv1	sum	1.0	0.0 1
20525101 0.0	1.05331	htrnr	200000100
20525102 0.79000	htrnr	200100101	
20525103 1.01501	htrnr	200100201	
20525104 2.29335	htrnr	200100301	
20525105 2.29335	htrnr	200100401	
20525106 2.29335	htrnr	200100501	
20525107 2.29335	htrnr	200100601	
20525108 1.33475	htrnr	205000100	
20525109 1.93518	htrnr	205000101	
20525110 2.82907	htrnr	210000100	
20525111 2.82907	htrnr	210000200	
20525112 2.82907	htrnr	210000300	
20525113 2.82907	htrnr	210000400	
20525114 1.06311	htrnr	210000500	
20525115 1.09265	htrnr	210000600	
20525116 4.37241	htrnr	210000101	
20525117 4.37241	htrnr	210000201	
20525118 4.37241	htrnr	210000301	
20525119 4.37241	htrnr	210000401	
20525120 1.64308	htrnr	210000501	
*			
20525200 rv2	sum	1.0	0.0 1
20525201 0.0	1.68872	htrnr	210000601
20525202 1.95223	htrnr	211000100	
20525203 4.41094	htrnr	211000200	
20525204 2.99281	htrnr	211000300	
20525205 1.41813	htrnr	212000100	
20525206 4.41094	htrnr	212000200	
20525207 4.41094	htrnr	212000300	
20525208 1.65755	htrnr	212000400	
20525209 1.70360	htrnr	212000500	
20525210 1.6800	htrnr	220000100	
*			
20525300 rv3	sum	1.0	0.0 1
20525301 0.0	0.695734	htrnr	225000700
20525302 0.921366	htrnr	226000100	
20525303 1.98094	htrnr	240000100	
20525304 1.80000	htrnr	246000100	
20525305 1.80000	htrnr	246000101	
20525306 2.04439	htrnr	250000100	
20525307 1.00000	htrnr	251000100	
20525308 1.00000	htrnr	251000200	
20525309 1.70445	htrnr	250100100	
20525310 0.71200	htrnr	255000100	
20525311 1.68000	htrnr	220000101	
20525312 0.980177	htrnr	225000100	
20525313 1.05369	htrnr	225000200	
20525314 1.05369	htrnr	225000300	
20525315 1.23842	htrnr	225000400	
20525316 2.10738	htrnr	225000500	
20525317 0.791681	htrnr	225000600	
20525318 1.0	cntrlvar	251	

20525319	1.0	cntrlvar	252		20513006	0.12452	htnr	315300200			
*----1----	-----1----	-----1----	-----1----		20513007	0.12452	htnr	315300300			
* metal heating in broken loop (1st part)					20513008	0.12452	htnr	315300400			
*----1----	-----1----	-----1----	-----1----		20513009	0.12452	htnr	315300500			
20512600	bklpmht	sum	1.0	0.0	1	20513010	0.12452	htnr	315300600		
20512601	0.0	0.157878	htnr	300000100		20513011	0.04239	htnr	315400100		
20512602		0.622764	htnr	300000200		20513012	0.04363	htnr	315500100		
20512603		1.27051	htnr	300000300	*----1----	-----1----	-----1----	-----1----			
20512616		0.668713	htnr	335000100	* metal heating in steam generator						
20512617		0.622764	htnr	335000200	*----1----	-----1----	-----1----	-----1----			
20512618		0.869015	htnr	335000300		20555100	sgmth1	sum	1.0	0.0	1
*----1----	-----1----	-----1----	-----1----		20555101	0.0	1.47943	htnr	500000100		
* metal heating in broken loop					20555102		1.47943	htnr	500000200		
*----1----	-----1----	-----1----	-----1----		20555103		0.291097	htnr	500000300		
20512700	bklpmpt	sum	1.0	0.0	1	20555104		1.52566	htnr	500000101	
20512701	0.0	1.39487	htnr	370000100		20555105		1.52566	htnr	500000201	
20512702		0.771131	htnr	370000200		20555106		0.300194	htnr	500000301	
20512703		0.768435	htnr	370000300		20555107		0.615526	htnr	515000100	
20512704		2.12160	htnr	370000400		20555108		2.88042	htnr	515000200	
20512705		1.0	cntrlvar	126		20555109		2.88042	htnr	515000300	
*----1----	-----1----	-----1----	-----1----			20555110		2.88042	htnr	515000400	
* metal heating in intact loop hot leg						20555111		0.627655	htnr	515000101	
*----1----	-----1----	-----1----	-----1----			20555112		2.93718	htnr	515000201	
20512800	ihlmht	sum	1.0	0.0	1			2.93718	htnr	515000301	
20512801	0.0	1.3716	htnr	100100100				2.93718	htnr	515000401	*
20512802		1.45787	htnr	100100200							
20512803		0.55548	htnr	100100300		20555200	sgmth2	sum	1.0	0.0	1
20512804		1.28345	htnr	100100400		20555201	0.0	3.40507	htnr	530000100	
20512805		0.72288	htnr	100200100		20555202		3.40507	htnr	530000200	
20512806		1.4772	htnr	100400100		20555203		3.20846	htnr	530000300	
*----1----	-----1----	-----1----	-----1----			20555204		3.30846	htnr	530000400	
* metal heating in intact loop cold leg						20555205		2.31474	htnr	530000500	
*----1----	-----1----	-----1----	-----1----			20555206		3.17360	htnr	530000600	
20512900	ildmht	sum	1.0	0.0	1			3.17360	htnr	530000700	
20512901	0.0	0.614734	htnr	100100500							
20512902		0.498747	htnr	100100600		*----1----	-----1----	-----1----	-----1----		
20512903		0.678081	htnr	100100700		* pcs-tubesheet heat transfer					
20512904		0.443073	htnr	100100800		*----1----	-----1----	-----1----	-----1----		
20512905		0.498747	htnr	100100900		20513200	pcstub	sum	1.0	0.0	1
20512906		0.546926	htnr	100101000		20513201	0.0	56.4226	htnr	115100100	
20512907		0.625441	htnr	100101100		20513202		56.4226	htnr	115100200	
20512908		1.30352	htnr	100101200		20513203		0.157962	htnr	115200100	
20512909		0.558497	htnr	100200200		20513204		0.157962	htnr	115200200	
20512910		0.678584	htnr	100300100		*----1----	-----1----	-----1----	-----1----		
20512911		0.310113	htnr	100300200		* tubesheet-scs heat transfer					
20512912		0.340649	htnr	100300300		*----1----	-----1----	-----1----	-----1----		
20512913		0.955718	htnr	100300400		20513300	tushscs	sum	1.0	0.0	1
20512914		0.680620	htnr	100300500		20513301	0.0	0.157962	htnr	115200101	
20512915		0.310113	htnr	100300600		20513302		0.157962	htnr	115200201	
20512916		0.348792	htnr	100300700		*----1----	-----1----	-----1----	-----1----		
20512917		1.4772	htnr	100400200		* metal hx in rabs					
*----1----	-----1----	-----1----	-----1----		*----1----	-----1----	-----1----	-----1----			
* metal heating in broken loop simulators					20517000	rabs	sum	1.0	0.0	1	
*----1----	-----1----	-----1----	-----1----		20517001	0.0	1.39487	htnr	370000100		
20513000	blhisim	sum	1.0	0.0	1	20517002		0.77113	htnr	370000200	
20513001	0.0	0.1312	htnr	315000100		20517003		0.77278	htnr	370000300	
20513002		0.1703	htnr	315000200		20517004		2.12160	htnr	370000400	
20513003		0.0042	htnr	315100100		*****					
20513004		0.00347	htnr	315200100		* bl total metal hx					
20513005		0.12452	htnr	315300100							

*****						
20517100	qbtotal	sum	1.0	0.0	1	
20517101	0.0	1.0	cntrlvar	127		
*20517102		1.0	cntrlvar	170		
20517103		1.0	cntrlvar	130	* only for simula	
*****						
* pcs stored energy excluding pressurizer						
*****						
20557000	pcsqre sum	1.0	0.0	1		
20557001	0.0	1.0	cntrvar	253	* rv metal heat	
20557002		1.0	cntrvar	113	* rv ambloss	
20557003		1.0	cntrvar	171	* only for simula	
20557004		1.0	cntrvar	117	* blhl ambloss	
20557005		1.0	cntrvar	118	* blcl ambloss	
20557006		1.0	cntrvar	119	* rabv ambloss	
20557007		1.0	cntrvar	128	* ilhl heat	
20557008		1.0	cntrvar	120	* ilhl ambloss	
20557009		1.0	cntrvar	129	* ild heat	
20557010		1.0	cntrvar	121	* ild ambloss	
20557011		1.0	cntrvar	132	* pcs-tubesheet	
20557012		1.0	cntrvar	133	* tubesheet-scs	
*****						
* scs stored energy						
*****						
20557300	scsqse sum	1.0	0.0	1		
20557301	0.0	1.0	cntrvar	552	* sg heat	
20557302		1.0	cntrvar	115	* sg ambloss	
*****						
* heat flow calculations						
*****						
* ecc energy flow						
*****						
20515300	pvecc	div	1.0	0.0	1	
20515301		rhofj	630000000	p	600010000	
20515400	hecc	sum	1.0	0.0	1	
20515401	0.0	1.0	ufj	630000000		
20515402		1.0	cntrvar	153		
20515500	mdothecc	mult	1.0	0.0	1	
20515501		mflowj	630000000			
20515502		cntrvar	154			
20515600	qecc/v	mult	0.126646	0.0	1	
20515601		cntrvar	155			
20515700	mdotev	mult	0.126646	0.0	1	
20515701		mflowj	630000000			
*****						
* sg hx per unit pcs volume						
*****						
20516000	qsg/v	mult	0.126646	0.0	1	
20516001		cntrvar	112			
*****						
* core hx per unit pcs volume						
*****						
20516100	qcore/v	mult	0.126646	0.0	1	
20516101		cntrvar	111			
*****						
* pump power						
*****						
20516200	p1edotv	mult	0.04136	0.0	1	
20516201		voidgj	135020000			
20516202		velgj	135020000			
20516203						
20516300	p1edotl	mult	0.04136	0.0	1	
20516301		voidfj	135020000			
20516302		velfj	135020000			
20516303		pmphead	135			
20516400	p2edotv	mult	0.04136	0.0	1	
20516401		voidgj	165020000			
20516402		velgj	165020000			
20516403		pmphead	165			
20516500	p2edotl	mult	0.04136	0.0	1	
20516501		voidfj	165020000			
20516502		velfj	165020000			
20516503		pmphead	165			
20516600	qpmp	sum	1.0	0.0	1	
20516601	0.0	1.0	cntrvar	162		
20516602		1.0	cntrvar	163		
20516603		1.0	cntrvar	164		
20516604		1.0	cntrvar	165		
20516700	qpmp/v	mult	0.126646	0.0	1	
20516701		cntrvar	166			
*****						
* energy to fluid in vessel from structures						
*****						
20562000	rvhx	sum	6.2832	0.0	1	
20562001	0.0	0.3080	htmr	205000101		
20562002		0.6959	htmr	210000101		
20562003		0.6959	htmr	210000201		
20562004		0.6959	htmr	210000301		
20562005		0.6959	htmr	210000401		
20562006		0.2615	htmr	210000501		
20562007		0.2688	htmr	210000601		
20562008		0.3107	htmr	211000100		
20562009		0.7020	htmr	211000200		
20562010		0.7020	htmr	212000100		
20562011		0.7020	htmr	212000200		
20562012		0.7030	htmr	212000300		
20562013		0.6	htmr	212000400		
20562014		0.2	htmr	212000500		
20562015		1.0	cntrvar	253		
*****						
* total vessel hx/v						
*****						
20562100	rvhx/v	mult	1.0	0.0	1	
20562101		cntrvar	620			
*****						
* total massless energy flows from pcs excluding qcore and qsg						
*****						
20562200	qstruc	sum	1.0	0.0	1	
20562201	0.0	1.0	cntrvar	123	* przr	
20562202		1.0	cntrvar	620	* rv	
20562203		1.0	cntrvar	171	* bl	
20562204		1.0	cntrvar	128	* ilhl	
20562205		1.0	cntrvar	129	* lcl	
20562300	qstruc/v	mult	0.126646	0.0	1	
20562301		cntrvar	622			
*****						
* sum of all massless energy flows from pcs						
*****						
20562400	de/dt	sum	1.0	0.0	1	
20562401	0.0	1.0	cntrvar	111	* core	

20562402	1.0	cntrlvar	112	* sg		*----1----1----1----
20562403	1.0	cntrlvar	622	* structure		* spray valve position calculator
20562404	1.0	cntrlvar	166	* pumps		*----1----1----1----
20562500	de/dt/vv	mult	0.126646	0.0	1	20590400 spray sum -1.0 0.0 1 * contin
20562501	cntrlvar	624				+ 3 0.0 1.0
*****						20590401 14.93+6 -1.0 p 420010000
* sum of mass flow energy flows and massless energy flows						*----1----1----1----
*****						* position vs area table
20562600	dtqflo	sum	1.0	0.0	1	*----1----1----1----
20562601	0.0	1.0	cntrlvar	624	* de/dt	20299900 normarea
20562602	-1.0	cntrlvar	433	* porv		20299901 0.0 0.0
20562700	dtqf/v	mult	0.126646	0.0	1	20299902 0.0001 0.0
20562701	cntrlvar	626				20299903 1.0 1.0
*----1----1----1----1----1----1----						*----1----1----1----1----1----
* primary coolant pump speed controllers						* pressurizer level control using charging and letdown components
*----1----1----1----1----1----1----						*----1----1----1----1----1----
* calculate mass flow error						* charging reservoir
*----1----1----1----						*----1----1----1----
20590100	msserr	sum	1.0	0.0	1	*9800000 chrg tmddpvol
20590101	479.30	-1.0	mflowj	100010000		*9800101 1.0 1.0 0.0 0.0 0.0 0.0
*----1----1----1----						*9800102 4.0-5 0.0 00000
* pump 1 speed						*9800200 3
*----1----1----1----						*9800201 0.0 2.07+07 558.9
20590200	pcp1spd	integral	0.34482	333.7236	1	*----1----1----1----
20590201	cntrlvar	901				* charging valve
*----1----1----1----						*----1----1----1----
* pcp1 pump velocity table						*9850000 chrg valve
*----1----1----1----						*9850101 980000000 185000000 3.8e-05 0.0 0.0 000100
1356100	508	cntrlvar	902			*9850201 0 .00000000 .00000000 0.0
1356101	0.0	0.0				*9850300 srvalv
1356102	369.0	369.0				*9850301 905 999
*----1----1----1----						*----1----1----1----
* modify pcp1 pump data						* charging valve position calculator
*----1----1----1----						*----1----1----1----
1350301	0	0	0	-1	0	504 0 *20590500 charge sum 7.7 0.0 1
*----1----1----1----						*contin
* pump 2 speed						+ 3 0.0 1.0
*----1----1----1----						*20590501 0.92 -1.0 cntrlvar 2
20590300	pcp2spd	integral	0.34482	331.9524	1	*----1----1----1----
20590301	cntrlvar	901				* letdown sink
*----1----1----1----						*----1----1----1----
* pcp2 pump velocity table						*9900000 ltdwn tmddpvol
*----1----1----1----						*9900101 1.0 1.0 0.0 0.0 0.0 0.0
1656100	508	cntrlvar	903			*9900102 4.0-5 0.0 00000
1656101	0.0	0.0				*9900200 3
1656102	369.0	369.0				*9900201 0.0 1.4+7 558.9
*----1----1----1----						*----1----1----1----
* modify pcp2 pump data						* letdown valve
*----1----1----1----						*----1----1----1----
1650301	135	135	135	-1	0	504 0 *9950000 ltdwn valve
*----1----1----1----1----1----						*9950101 185000000 990000000 2.5-5 0.0 0.0 000100
* pressurizer spray valve controller						*9950201 0 .00000000 .00000000 0.0
*----1----1----1----1----1----						*9950300 srvalv
* spray valve						*9950301 906 999
*----1----1----1----						*----1----1----1----
4070000	sprvalv	valve				* letdown valve position calculator
4070101	406010000	420010000	3.3451e-4	1.2	1.2	000100 *----1----1----1----
4070201	0	.00000000	.00000000	0.0		*20590600 letdown sum -7.7 0.0 1
4070300	srvalv					*contin
4070301	904	999				+ 3 0.0 1.0

```

*20590601 1.10     -1.0      cntrlvar 2
*----1---1---1---1---1---1---1---1---1---
* steam valve controller
*----1---1---1---1---1---1---1---1---
* changes to steam valve
*----1---1---1---1---
*5500201 0       19.758   22.082   0.0
*5500300 srvlv
*5500301 910     540
*20254000 normarea
*20254001 0.0     0.0
*20254002 0.0001  0.0
*20254003 1.0     1.0
*----1---1---1---1---
* compute delta t error
*----1---1---1---1---
*20590700 delta sum    1.0     0.0     1
*20590701 559.0    -1.      tempf   185010000
*----1---1---1---1---
* filter delta t thru deadband
*----1---1---1---1---
*20590800 deadband function 1.0     0.0     1
*20590801 cntrlvar 907     908
*20290800 reac-t
*20290801 -100.    -100.
*20290802 -0.25    -0.25
*20290803 -0.25    0.0
*20290804 0.25    0.0
*20290805 0.25    0.25
*20290806 100.    100.
*----1---1---1---1---
* integrate delta t error
*----1---1---1---1---
*20590900 int integral 1.0     0.0     1
*20590901 cntrlvar 908
*----1---1---1---1---
* steam valve position calculator
*----1---1---1---1---
*20591000 tcontrol sum    1.0     0.645229  0      *conti
*+      3       0.6     0.90
*20591001 0.645229  -0.07126  cntrlvar 908
*20591002          -0.01492  cntrlvar 909
*----1---1---1---1---1---1---1---1---
* simplified feed system controller
*----1---1---1---1---1---1---1---1---
20591100 sglvterr sum    1.0     0.0     1
20591101 3.09     -1.0      cntrlvar 001
20591200 feedflow sum    1.0     0.0     1
20591201 0.0      1.0      mflowj   550000000
20591202          48.4     cntrlvar 911
*----1---1---1---1---
* replace feed junction table
*----1---1---1---1---
5600200 1       0       cntrlvar 912
5600201 -100.0   25.553   0.0     0.0
5600202 -1.0     0.0     0.0     0.0
5600203 0.0      0.0     0.0     0.0
5600204 50.0     50.0     0.0     0.0
.

```



## **Appendix B**

### **Transient Input Deck for Base Case**



```

=loft l9-1 post test analysis deck
*----1----1----1----1----1----1----1----1----
*      initial conditions
*
*      pcp pressure = 14.901 mpa
*      core power = 50. mw
*      pcs flow = 479.3 kg/s
*      thot = 578. k
*      tcold = 559.0 k
*
*----1----1----1----1----1----1----1----
0000100  restart  transnt
0000101  run
0000102  si
0000103      15808
0000105  5.    10.
0000201  200.00   1.e-6   1.0     3   1   30   100
0000202  1000.0    1.e-6   1.0     3   5   300   500
0000203  2000.0    1.e-6   0.1     3   50   3000  5000
0000204  4000.0    1.e-6   0.5     3   10   1000  2000
0000205  8000.0    1.e-6   0.1     3   50   4000  5000
0000206  10000.0   1.e-6   0.5     3   10   2000  2000
*****
*      minor edit variables
*
***** pressure *****
0000301  p      310010000 * pe-bl-2
*0000303  p      315110000 * pe-bl-3
*0000304  p      350010000 * pe-bl-4
*0000305  p      315090000 * pe-bl-6
*0000306  p      350020000 * pe-bl-8
0000302  p      185010000 * pe-pc-1
0000303  p      100010000 * pe-pc-2
0000304  p      420010000 * porv inlet
*0000310  p      110010000 * pt-139-2,3,4
0000305  p      245010000 * pe-1up-1a,1b
0000306  p      215010000 * pe-1st-1a,b/pe-2st-1a,b
*0000313  p      200010000 * pe-1st-3a,3b
0000307  p      530010000 * pe-sgs-01
0000308  p      535010000 * pt-p4-85
***** temperatures *****
0000309  tempf   406010000 * spray tempf
0000310  tempf   310010000 * te-bl-2a,2b,2c
0000311  tempf   100010000 * te-pc-2a,2b,2c
0000312  tempf   185010000 * te-pc-1
0000313  tempf   115030000 * te-sg-1
0000314  tempf   115100000 * te-sg-2
0000315  tempf   515070000 * te-sg-4
*0000328  tempf   415050000 * pqr volume 5
0000316  tempf   415040000 * te-139-19
*0000330  tempf   415030000 * te-139-20
*0000331  tempf   315120000 * te-p138-171
*0000332  tempf   350020000 * te-p138-170
*0000333  tempf   205010000 * te-1st-1/te-2st-1
0000317  tempf   210010000 * te-1st-2/te-2st-2
*0000335  tempf   345010000 * te-bl-1
*0000336  tempf   210030000 * te-1st-14/te-2st-14
*0000337  tempf   210040000 * te-3up-2
*0000338  tempf   245010000 * te-1up-6
*0000339  tempf   246010000 * te-2up-4
*0000340  tempf   250010000 * te-1up-3
***** densities *****

```

```

*****0000341 rho      345010000 * de-bl-1
0000318 rho      310010000 * de-bl-2
0000319 rho      185010000 * de-pc-1
0000320 rho      100010000 * de-pc-2
*0000345 rho      115120000 * de-pc-3
0000321 voidgj   400010000 * surge line density
*0000347 rho      115040000 * s/g tubes
*0000348 rho      115050000 * s/g tubes
*0000349 rho      115060000 * s/g tubes
*0000350 rho      115070000 * s/g tubes
*****velocities
*****0000351 voidf    100010000 * ihl nozzle
*0000352 velf     100010000 * ihl nozzle
*0000353 velf     115030000 * s/g inlet
*0000354 velf     400010000 * surge line
*0000355 velfj    425000000 * porv liq vel
*0000356 velg     100010000 * ihl nozzle
*0000357 velg     115030000 * s/g inlet
*0000358 velg     400010000 * surge line
*0000359 velgj    425000000 * porv vap vel
*****mass flow rates
*****0000322 mflowj   100010000 * ihl nozzle
*0000361 mflowj   150010000 * pump outlet
*0000362 mflowj   185020000 * dtt-rake ild
0000323 mflowj   400010000 * pres. surge line flow
0000324 mflowj   407000000 * pzt spray flow
0000325 mflowj   425000000 * pres. relief valve flow
0000326 mflowj   550000000 * steam flow control valve
0000327 mflowj   548000000 * aux feed
*0000369 mflowj   560000000 * main feed
*****cladding temperatures center module
*****0000371 httemp   230000110 * te-5h5-015
*0000372 httemp   230000210 * te-5h5-034
*0000373 httemp   230000310 * te-5h5-049
*****peak centerline temperatures
*****0000374 httemp   230000101 * core lower region
*0000375 httemp   230000201 * core middle region
*0000376 httemp   230000301 * core upper region
*****reactor kinetic parameters
*****
0000328 rktpow   0      * total reactor power
*0000378 rkfpow   0      * fission decay power
*0000379 rkgapow  0      * gamma decay power
*0000380 rkreac   0      * reactivity
*0000381 pmphead  135   * pcp1 head
*0000382 pmphead  165   * pcp2 head
0000329 mflowj   185010000
0000330 mflowj   185030000
*0000388 mflowj   200020000
0000331 pmpvel   135
*****control variable requests
*****0000332 cntrlvar  001
0000333 cntrlvar  002
0000334 cntrlvar  003
0000335 cntrlvar  041
0000336 cntrlvar  042
0000337 cntrlvar  043
0000338 cntrlvar  004
0000339 cntrlvar  005
0000340 cntrlvar  006
0000341 cntrlvar  007
0000342 cntrlvar  008
0000343 cntrlvar  009

```

```

0000344 cntrlvar 010
0000345 cntrlvar 433
0000346 cntrlvar 434
0000347 cntrlvar 111
0000348 cntrlvar 112
0000349 cntrlvar 113
0000350 cntrlvar 114
0000351 cntrlvar 115
0000352 cntrlvar 116
0000353 cntrlvar 117
0000354 cntrlvar 118
0000355 cntrlvar 119
0000356 cntrlvar 120
0000357 cntrlvar 121
0000358 cntrlvar 122
0000359 cntrlvar 123
0000360 cntrlvar 251
0000361 cntrlvar 252
0000362 cntrlvar 253
0000363 cntrlvar 126
0000364 cntrlvar 127
0000365 cntrlvar 128
0000366 cntrlvar 129
0000367 cntrlvar 130
0000368 cntrlvar 551
0000369 cntrlvar 552
0000370 cntrlvar 132
0000371 cntrlvar 133
0000372 cntrlvar 170
0000373 cntrlvar 171
0000374 cntrlvar 570
0000375 cntrlvar 573
0000376 cntrlvar 153
0000377 cntrlvar 154
0000378 cntrlvar 155
0000379 cntrlvar 156
0000380 cntrlvar 157
0000381 cntrlvar 160
0000382 cntrlvar 161
0000383 cntrlvar 166
0000384 cntrlvar 167
0000385 cntrlvar 620
0000386 cntrlvar 621
0000387 cntrlvar 622
0000388 cntrlvar 623
0000389 cntrlvar 624
0000390 cntrlvar 625
0000391 cntrlvar 626
0000392 cntrlvar 627
0000393 tempg 515070000
0000394 rho 420010000
0000395 cputime 0
20800095 dt 0
20800096 dtcrnt 0
*****
* trips
*
***** variable trips *****
*****0000501 p 100010000 le null 0 14.193103e6 l
* ecc check valve
0000502 p 600010000 ge p 185010000 20.e6 n
* accumulator check valve
0000503 p 615010000 ge p 185010000 20.e6 n

```

```

*      isolation valve hot leg
0000504 time 0      lt null 0      0.0      i
*      isolation valve cold leg
0000505 time 0      lt null 0      0.0      i
*      qobv hot leg
0000506 time 0      lt null 0      0.0      i
*      qobv cold leg
0000507 time 0      lt null 0      0.0      i
*      check valve surge line pressurizer
0000508 time 0      ge null 0      0.0      i
*      pressurizer relief valve
0000509 tempf 100010000 ge null 0      597.0      i
*      steam control valve
0000510 time 0      lt null 0      0.0      i
*      boundary system valve
0000511 time 0      lt null 0      0.0      i
*      lpis trip
0000512 time 0      ge null 0      10000.0      i
*      hpis trip
0000513 time 0      ge null 0      10000.0      i
*
0000520 p    530020000 gt null 0      7.103448e6 n
0000521 p    530020000 lt null 0      7.0344827e6 n
0000522 p    530020000 gt null 0      6.3448275e6 n
0000523 p    530020000 lt null 0      6.4137931e6 n
0000530 time 0      ge null 0      3600.0      n
0000531 p    530020000 gt p    547010000 0.0      n
0000536 time 0      ge null 0      10000.0      n
0000540 tempf 100010000 gt null 0      583.16      i
0000541 p    100010000 gt null 0      1.574553e7 i
0000550 time 0      ge null 0      10000.0      i
0000551 time 0      ge timeof 625      0.0      i
0000552 time 0      ge timeof 509      1580.      i
0000560 p    100010000 le null 0      13.15862e6 n
0000561 time 0      ge timeof 552      265.0      i
0000562 time 0      gt null 0      5400.0      n
0000563 cntrvar 1      lt null 0      2.1844      n
0000564 cntrvar 1      gt null 0      2.9464      n
0000565 time 0      ge timeof 669      966.      i
0000570 p    420010000 gt null 0      1.620058e7 n
0000571 p    420010000 lt null 0      1.606269e7 n
0000572 p    420010000 lt null 0      1.486300e7 n
0000573 p    420010000 gt null 0      1.506980e7 n
0000574 p    420010000 gt null 0      1.533874e7 n
0000575 p    420010000 lt null 0      1.505000e7 n
0000576 p    420010000 lt null 0      1.482853e7 n
0000577 p    420010000 gt null 0      1.495950e7 n
***** logical trips
*****0000600 536
0000601 563 and 561 n
0000602 -563 and -564 n
0000603 655 and 602 n
0000604 609 or 609 i
0000605 572 and -509 n
0000606 -572 and -573 n
0000607 608 and 606 n
0000608 605 or 607 n
0000609 540 or 541 i
0000610 612 or 520 n
0000611 -521 and -616 n
0000612 611 and 610 n
0000613 616 or 523 n
0000614 -522 and 613 n

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0000615 -612      and    609      n
0000616  615      and    614      n
0000617  612      or     616      n
0000618  605      or     607      n
0000621  623      or     570      n
0000622 -571      and    -571     n
0000623  621      and    622      n
0000624  509      and    -552     n
0000625  623      or     624      n
0000626  576      and    -509     n
0000627 -576      and    -577     n
0000628  629      and    627      n
0000629  626      or     628      n
0000635  504      and    504      n
0000636  509      and    -536     n
0000650 -652      and    550      n
0000651  650      or     652      n
0000652 -509      and    651      n
0000655  601      or     603      n
0000656  508      or     609      n
0000659  561      or     562      n
0000660  504      or     504      n
0000669  561      and    564      l
0000670  565      and    -655     n
0000680  530      or     530      n
0000688  690      or     574      n
0000689 -575      and    -551     n
0000690  688      and    689      n
* pzc heater delete
14201000 delete
14202000 delete
*----1----1----1----1
* control variable 114 re-define
*----1----1----1----1
20511400 pzcheat sum  1.0  0.0  1
20511401  0.0   0.362  htrnr  415100101
20511402          0.702464 htrnr  415200101
20511403          1.26381 htrnr  415200201
20511404          1.26381 htrnr  415200301
20511405          0.649152 htrnr  415200401
20511406          0.649152 htrnr  415200501
20511407          0.534688 htrnr  415200601
20511408          0.534688 htrnr  415200701
20511409          0.273063 htrnr  416200101
*----1----1----1----1
* control variable 123 redefine
*----1----1----1----1
20512300 pzc sum  1.0  0.  1
20512301  0.0   0.362  htrnr  415100100
20512302          0.59522 htrnr  415200100
20512303          1.07086 htrnr  415200200
20512304          1.07086 htrnr  415200300
20512305          0.550045 htrnr  415200400
20512306          0.550045 htrnr  415200500
20512307          0.453056 htrnr  415200600
20512308          0.453056 htrnr  415200700
20512309          0.150656 htrnr  416200100
***** primary coolant pump 1
*****1350000  pcpump1      pump
1350101  0.0366  0.0    0.099   0.0    90.0   0.319
1350102  00000
1350108  130010000 0.0   0.0    0.0    000100
1350109  140000000 0.0   0.05   0.05   000100

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1350200 0      14818100. 1242890. 2463900.0 0.0
1350201 0      8.8943000 9.2942000 0.0
1350202 0      8.8928000 8.1177000 0.0
1350301 0 0 0 -1 0 509 0
1350302 369.000 .90178860 .315500 96.0000 500.600 1.4310000
1350303 613.6 0.0 207.0000 0.0040000 19.598000 0.0
1350310 0.0 0.0 0.0
*
***** single phase head curves
***** head curve no. 1
*----1----1----1----1----1----1----1----
1351100 1      1
1351101 0.000000e+00 1.403600e+00
1351102 1.906100e-01 1.363600e+00
1351103 3.896300e-01 1.318600e+00
1351104 5.939600e-01 1.232800e+00
1351105 7.902000e-01 1.133600e+00
1351106 1.000000e+00 1.000000e+00
*----1----1----1----1----1----1----1----
* head curve no. 2
*----1----1----1----1----1----1----1----
1351200 1      2
1351201 0.000000e+00 -6.700000e-01
1351202 2.000000e-01 -5.000000e-01
1351203 4.000000e-01 -2.500000e-01
1351204 5.755400e-01 0.000000e+00
1351205 7.443200e-01 2.583000e-01
1351206 7.734800e-01 3.778000e-01
1351207 8.631300e-01 6.326000e-01
1351208 1.000000e+00 1.000000e+00
*----1----1----1----1----1----1----1----
* head curve no. 3
*----1----1----1----1----1----1----1----
1351300 1      3
1351301 -1.000000e+00 2.472200e+00
1351302 -8.057400e-01 2.047400e+00
1351303 -6.069000e-01 1.831000e+00
1351304 -4.068300e-01 1.624000e+00
1351305 -2.001710e-01 1.470500e+00
1351306 0.000000e+00 1.403600e+00
*----1----1----1----1----1----1----1----
* head curve no. 4
*----1----1----1----1----1----1----1----
1351400 1      4
1351401 -1.000000e+00 2.472200e+00
1351402 -8.229700e-01 1.996800e+00
1351403 -6.333200e-01 1.589700e+00
1351404 -4.553400e-01 1.327900e+00
1351405 -2.710900e-01 1.194900e+00
1351406 -1.771600e-01 1.060500e+00
1351407 -9.073000e-02 1.015600e+00
1351408 0.000000e+00 9.342790e-01
*----1----1----1----1----1----1----1----
* head curve no. 5
*----1----1----1----1----1----1----1----
1351500 1      5
1351501 0.000000e+00 2.500000e-01
1351502 2.000000e-01 2.800000e-01
1351503 4.000000e-01 3.400000e-01
1351504 4.118000e-01 2.768000e-01
1351505 5.976300e-01 4.584000e-01
1351506 7.934670e-01 6.992000e-01
1351507 1.000000e+00 1.000000e+00

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1352105 -1.992800e-01    6.648000e-01
1352106  0.000000e+00    6.032000e-01
*----1----1----1----1----1----1----1---
* torque curve no. 4
*----1----1----1----1----1----1---
1352200  2                  4
1352201 -1.000000e+00    1.984300e+00
1352202 -8.223400e-01    1.830800e+00
1352203 -6.337100e-01    1.682400e+00
1352204 -4.585300e-01    1.557000e+00
1352205 -2.670230e-01    1.436200e+00
1352206 -1.761070e-01    1.387900e+00
1352207 -8.931000e-02    1.348100e+00
1352208  0.000000e+00    1.233610e+00
*----1----1----1----1----1----1----1---
* torque curve no. 5
*----1----1----1----1----1----1---
1352300  2                  5
1352301  0.000000e+00    -4.500000e-01
1352302  4.000000e-01    -2.500000e-01
1352303  5.000000e-01    0.000000e+00
1352304  1.000000e+00    3.569000e-01
*----1----1----1----1----1----1----1---
* torque curve no. 6
*----1----1----1----1----1----1---
1352400  2                  6
1352401  0.000000e+00    1.233610e+00
1352402  9.064300e-02    1.196500e+00
1352403  1.885690e-01    1.109600e+00
1352404  2.734700e-01    1.041600e+00
1352405  4.586690e-01    8.958000e-01
1352406  5.744800e-01    7.807000e-01
1352407  7.381600e-01    6.134000e-01
1352408  7.685200e-01    5.849000e-01
1352409  8.700570e-01    4.877000e-01
1352410  1.000000e+00    3.569000e-01
*----1----1----1----1----1----1----1---
* torque curve no. 7
*----1----1----1----1----1----1---
1352500  2                  7
1352501 -1.000000e+00    -1.000000e+00
1352502 -3.000000e-01    -9.000000e-01
1352503 -1.000000e-01    -5.000000e-01
1352504  0.000000e+00    -4.500000e-01
*----1----1----1----1----1----1----1---
* torque curve no. 8
*----1----1----1----1----1----1---
1352600  2                  8
1352601 -1.000000e+00    -1.000000e+00
1352602 -2.500000e-01    -9.000000e-01
1352603 -8.000000e-02    -8.000000e-01
1352604  0.000000e+00    -6.700000e-01
***** two - phase multiplier data from l9-1 test data
***** head curve
*----1----1----1----1----1----1---
1353000  0
1353001  0.000000e+00    0.000000e+00
1353002  2.000000e-02    2.000000e-02
1353003  6.000000e-02    5.000000e-02
1353004  1.000000e-01    1.000000e-01
1353005  2.000000e-01    4.600000e-01
1353006  2.400000e-01    8.000000e-01
1353007  3.000000e-01    9.600000e-01

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1353008 4.000000e-01    9.800000e-01
1353009 6.000000e-01    9.700000e-01
1353010 8.000000e-01    9.000000e-01
1353011 9.000000e-01    8.000000e-01
1353012 9.600000e-01    5.000000e-01
1353013 1.000000e+00    0.000000e+00
*----1----1----1----1----1----1----1----
* torque curve
*----1----1----1----1----1----1----1----
1353100 0
1353101 0.000000e+00    0.000000e+00
1353102 1.250000e-01    7.000000e-02
1353103 1.650000e-01    1.250000e-01
1353104 2.400000e-01    5.600000e-01
1353105 8.000000e-01    5.600000e-01
1353106 9.600000e-01    4.500000e-01
1353107 1.000000e+00    0.000000e+00
***** pump 2-phase difference data
***** head curve no. 1
*----1----1----1----1----1----1----1----
1354100 1                1
1354101 0.000000e+00    0.000000e+00
1354102 1.000000e-01    8.300000e-01
1354103 2.000000e-01    1.090000e+00
1354104 5.000000e-01    1.020000e+00
1354105 7.000000e-01    1.010000e+00
1354106 9.000000e-01    9.400000e-01
1354107 1.000000e+00    1.000000e+00
*----1----1----1----1----1----1----1----
* head curve no. 2
*----1----1----1----1----1----1----1----
1354200 1                2
1354201 0.000000e+00    0.000000e+00
1354202 1.000000e-01    -4.000000e-02
1354203 2.000000e-01    0.000000e+00
1354204 3.000000e-01    1.000000e-01
1354205 4.000000e-01    2.100000e-01
1354206 8.000000e-01    6.700000e-01
1354207 9.000000e-01    8.000000e-01
1354208 1.000000e+00    1.000000e+00
*----1----1----1----1----1----1----1----
* head curve no. 3
*----1----1----1----1----1----1----1----
1354300 1                3
1354301 -1.000000e+00   -1.160000e+00
1354302 -9.000000e-01   -1.240000e+00
1354303 -8.000000e-01   -1.770000e+00
1354304 -7.000000e-01   -2.360000e+00
1354305 -6.000000e-01   -2.790000e+00
1354306 -5.000000e-01   -2.910000e+00
1354307 -4.000000e-01   -2.670000e+00
1354308 -2.500000e-01   -1.690000e+00
1354309 -1.000000e-01   -5.000000e-01
1354310 0.000000e+00    0.000000e+00
*----1----1----1----1----1----1----1----
* head curve no. 4
*----1----1----1----1----1----1----1----
1354400 1                4
1354401 -1.000000e+00   -1.160000e+00
1354402 -9.000000e-01   -7.800000e-01
1354403 -8.000000e-01   -5.000000e-01
1354404 -7.000000e-01   -3.100000e-01
1354405 -6.000000e-01   -1.700000e-01

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1354406	-5.000000e-01	-8.000000e-02
1354407	-3.500000e-01	0.000000e+00
1354408	-2.000000e-01	5.000000e-02
1354409	-1.000000e-01	8.000000e-02
1354410	0.000000e+00	1.100000e-01
*----1----1----1----1----1----1----		
* head curve no. 5		
*----1----1----1----1----1----1----		
1354500	1	5
1354501	0.000000e+00	0.000000e+00
1354502	2.000000e-01	-3.400000e-01
1354503	4.000000e-01	-6.500000e-01
1354504	6.000000e-01	-9.300000e-01
1354505	8.000000e-01	-1.190000e+00
1354506	1.000000e+00	-1.470000e+00
*----1----1----1----1----1----1----		
* head curve no. 6		
*----1----1----1----1----1----1----		
1354600	1	6
1354601	0.000000e+00	1.100000e-01
1354602	1.000000e-01	1.300000e-01
1354603	2.500000e-01	1.500000e-01
1354604	4.000000e-01	1.300000e-01
1354605	5.000000e-01	7.000000e-02
1354606	6.000000e-01	-4.000000e-02
1354607	7.000000e-01	-2.300000e-01
1354608	8.000000e-01	-5.100000e-01
1354609	9.000000e-01	-9.100000e-01
1354610	1.000000e+00	-1.470000e+00
*----1----1----1----1----1----1----		
* head curve no. 7		
*----1----1----1----1----1----1----		
1354700	1	7
1354701	-1.000000e+00	0.000000e+00
1354702	0.000000e+00	0.000000e+00
*----1----1----1----1----1----1----		
* head curve no. 8		
*----1----1----1----1----1----1----		
1354800	1	8
1354801	-1.000000e+00	0.000000e+00
1354802	0.000000e+00	0.000000e+00
*----1----1----1----1----1----1----		
* torque curve no. 1		
*----1----1----1----1----1----1----		
1354900	2	1
1354901	0.000000e+00	6.032000e-01
1354902	1.930000e-01	6.325000e-01
1354903	3.930000e-01	7.369000e-01
1354904	5.955200e-01	8.331000e-01
1354905	7.978200e-01	9.229000e-01
1354906	1.000000e+00	1.000000e+00
*----1----1----1----1----1----1----		
* torque curve no. 2		
*----1----1----1----1----1----1----		
1355000	2	2
1355001	0.000000e+00	-6.700000e-01
1355002	4.000000e-01	-2.500000e-01
1355003	5.000000e-01	1.500000e-01
1355004	7.372550e-01	5.265860e-01
1355005	7.680490e-01	6.065940e-01
1355006	8.672300e-01	7.436600e-01
1355007	1.000000e+00	1.000000e+00
*----1----1----1----1----1----1----		

\* torque curve no. 3

\*----1----1----1----1----1----1----1----

1355100	2	3
1355101	-1.000000e+00	1.984300e+00
1355102	-8.009600e-01	1.394000e+00
1355103	-6.063800e-01	1.097500e+00
1355104	-4.068600e-01	8.220000e-01
1355105	-1.992800e-01	6.648000e-01
1355106	0.000000e+00	6.032000e-01

\*----1----1----1----1----1----1----1----

\* torque curve no. 4

\*----1----1----1----1----1----1----

1355200	2	4
1355201	-1.000000e+00	1.984300e+00
1355202	-8.223400e-01	1.830800e+00
1355203	-6.337100e-01	1.682400e+00
1355204	-4.585300e-01	1.557000e+00
1355205	-2.670230e-01	1.436200e+00
1355206	-1.761070e-01	1.387900e+00
1355207	-8.931000e-02	1.348100e+00
1355208	0.000000e+00	1.233610e+00

\*----1----1----1----1----1----1----

\* torque curve no. 5

\*----1----1----1----1----1----1----

1355300	2	5
1355301	0.000000e+00	-4.500000e-01
1355302	4.000000e-01	-2.500000e-01
1355303	5.000000e-01	0.000000e+00
1355304	1.000000e+00	3.569000e-01

\*----1----1----1----1----1----1----

\* torque curve no. 6

\*----1----1----1----1----1----1----

1355400	2	6
1355401	0.000000e+00	1.233610e+00
1355402	9.064300e-02	1.196500e+00
1355403	1.885690e-01	1.109600e+00
1355404	2.734700e-01	1.041600e+00
1355405	4.586690e-01	8.958000e-01
1355406	5.744800e-01	7.807000e-01
1355407	7.381600e-01	6.134000e-01
1355408	7.685200e-01	5.849000e-01
1355409	8.700570e-01	4.877000e-01
1355410	1.000000e+00	3.569000e-01

\*----1----1----1----1----1----1----

\* torque curve no. 7

\*----1----1----1----1----1----1----

1355500	2	7
1355501	-1.000000e+00	-1.000000e+00
1355502	-3.000000e-01	-9.000000e-01
1355503	-1.000000e-01	-5.000000e-01
1355504	0.000000e+00	-4.500000e-01

\*----1----1----1----1----1----1----

\* torque curve no. 8

\*----1----1----1----1----1----1----

1355600	2	8
1355601	-1.000000e+00	-1.000000e+00
1355602	-2.500000e-01	-9.000000e-01
1355603	-8.000000e-02	-8.000000e-01
1355604	0.000000e+00	-6.700000e-01

\*\*\*\*\* pcp1 pump velocity table  
\*\*\*\*\*1356100 536

1356101	0.0	0.0
1356102	1.0	220.

```

***** primary coolant pump 2
*****1650000 pcpump2      pump
1650101 0.0366 0.0 0.099 0.0 90.0 0.319
1650102 00000
1650108 160010000 0.0 0.0 0.0 000100
1650109 170000000 0.0 0.1 0.1 000100
1650200 0 14832700. 1242890. 2463590.0 0.0
1650201 0 8.4974000 8.8872000 0.0
1650202 0 8.4959000 6.6507000 0.0
1650301 135 135 135 -1 135 509 0
1650302 369.00000 .89699187 .31550000 96.000000 500.60000 1.431
1650303 613.6 0.0 207.433 0.004 19.5980 0.0
1650310 0.0 0.0 0.0
*----1----1----1----1----1----1----1----
* spray valve
*----1----1----1----1----1----1----1----
4070000 sprvlv valve
4070101 406010000 420010000 3.3451e-4 1.0 1.0 000100
4070201 0 .000000 .000000 0.0
4070300 trpvlv
4070301 690
*----1----1----1----1----1----1----1----
* air cooled condenser
*----1----1----1----1----1----1----1----
5470000 conders tmdpvol
5470101 0.21677 17.67 0.0 0.0 0.0 0.0
5470102 4.e-5 0.0 00000
5470200 1 680
5470201 0.0 559.15 0.999
5470202 18000. 334.15 0.999
*----1----1----1----1----1----1----1----
* aux feed water
*----1----1----1----1----1----1----1----
5480000 auxfeed tmdpjun
5480101 553000000 510000000 0.10
5480200 1 655
5480201 -1.0 0.0 0.0 0.0
5480202 0.0 0.0 0.0 0.0
5480203 0.0 2.5207 0.0 0.0
*----1----1----1----1----1----1----1----
* main feed water valve
*----1----1----1----1----1----1----1----
5600000 mnfeed tmdpjun
5600101 545000000 510000000 0.05
5600200 1 656
5600201 0.0 26.533 26.533 0.0
5600202 0.0 0.0 0.0 0.0
***** core collapsed liquid level
*****20255000 normarea 0 1.0 1.0
*20255001 0.0 9.25e-3
*20255002 9.25e-3 9.25e-3
*20255003 1.0 1.0
***** reactor kinetics data
*
*****30000000 point separabl
30000001 gamma-ac 49.6e+6 0.0 348.43 1.0 0.556
30000002 ans79-1
***** delayed neutron constants
*****30000101 0.0349 0.01275
30000102 0.2035 0.03177
30000103 0.1848 0.1181

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30000104  0.4046   0.3160
30000105  0.1401   1.402
30000106  0.0321   3.914
***** power history
*****30000401  4.89e+7   70.      hr
***** reactivity curve numbers
*****30000011  609
***** moderator density reactivity table
*****30000501  0.62626e+3  -4.4769

30000502  0.66396e+3  -3.2923
30000503  0.71617e+3  -1.5692
30000504  0.76112e+3  -0.1692
30000505  0.76837e+3   0.04615
30000506  0.79157e+3   0.6923
30000507  0.81188e+3   1.2398
30000508  0.86263e+3   2.2415
30000509  0.93804e+3   3.9231
30000510  0.99749e+3   5.1077
***** doppler reactivity table
*****30000601  293.16    1.375

30000602  338.72    1.125
30000603  422.05    0.682
30000604  477.60    0.419
30000605  505.38    0.274
30000606  570.72    0.000
30000607  588.72   -0.075
30000608  695.83   -0.526
30000609  922.05   -1.386
30000610 1310.94   -2.543
30000611 1810.94   -3.865
30000612 2088.72   -4.502
30000613 2499.83   -5.392
30000614 3027.60   -6.417
***** volume weighting factors
***** moderator temperature feedback
*****30000701  230010000  0   0.31493  0.0

30000702 230020000  0   0.31493  0.0
30000703 230030000  0   0.37014  0.0
***** doppler feedback
*****30000801  2300001  0   0.43153  0.0

30000802 2300002  0   0.51686  0.0
30000803 2300003  0   0.05161  0.0
*----1----1----1----1----1----1---

* scram reactivity data
*----1----1----1----1----1----1---

20260900 "react" 609
20260901 0.0      0.0
20260902 0.5      -0.5
20260903 0.59     -3.13
20260904 0.65     -3.95
20260905 0.75     -6.27
20260906 0.83     -8.72
20260907 0.90     -12.00
20260908 0.97     -17.12
20260909 1.125    -20.67
20260910 1.213    -22.10
20260911 1.3      -22.78
20260912 1.4      -23.17
20260913 1.6      -23.32
20260914 60.0     -23.32
.

```